



UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT
COLORADO SCHOOL OF MINES



Research Summary

P&T EFFECTS ON FILTRATION EFFICIENCY OF NANOPOROUS MEDIA

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UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT

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Motivation

- Porous medium acts like a semi-permeable membrane
- Current models of production from nanoporous, unconventional reservoirs do not consider hindered transport
- Explore the potential of thermal methods to enhance recovery from nanoporous formations

Problem Statement

- The passage of larger particles in a fluid mixture is hindered by tight pore throats
- Filtration efficiency of a nanoporous medium is a function of pressure and temperature
- Drastically different approach from the conventional definition of filtration

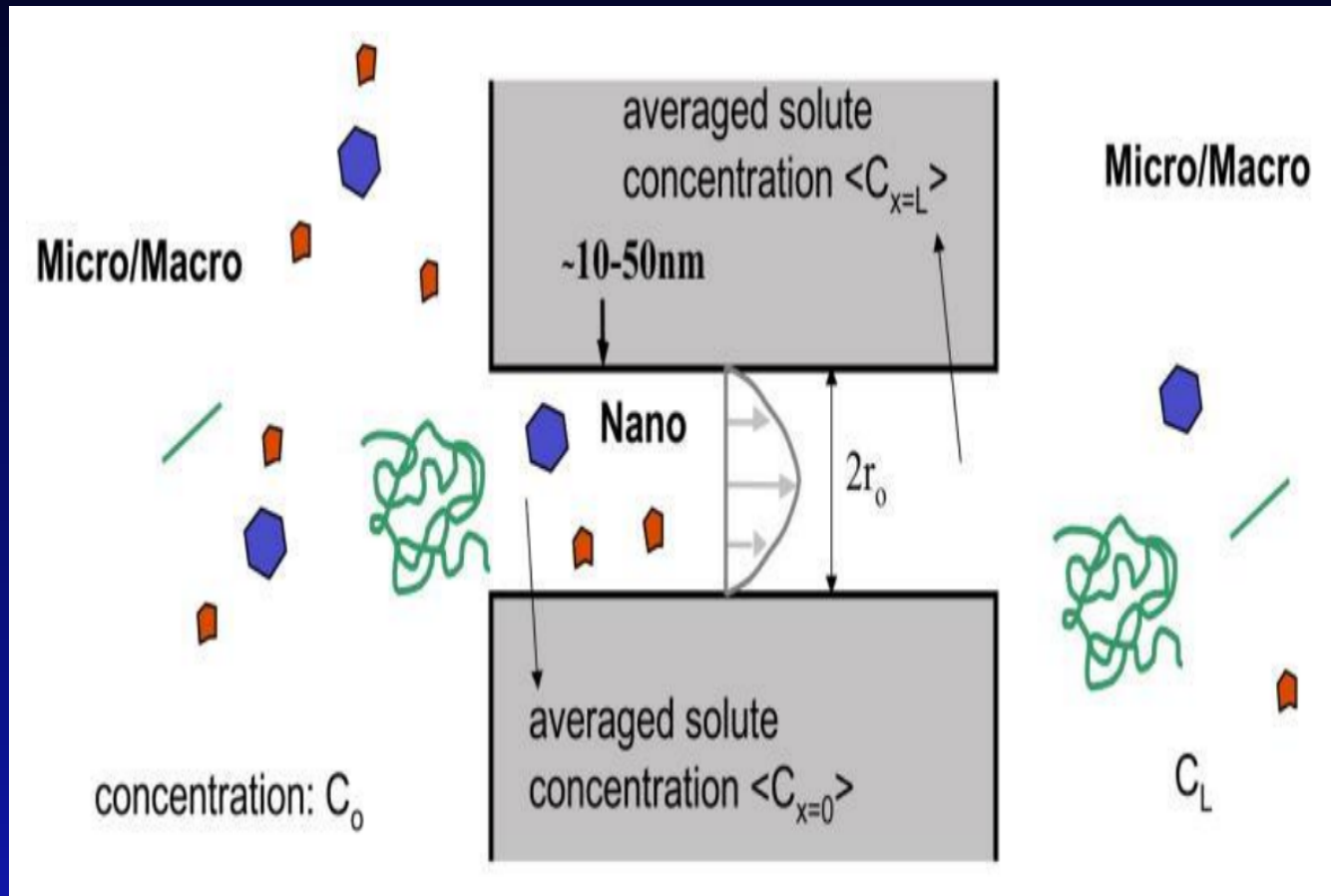
Objectives

Present:

- A filtration model based on the filtration efficiency concept
- The impact of temperature and pressure on filtration efficiency
- The possibility of thermal techniques to decrease filtration efficiency and increase recovery

Hindered Transport

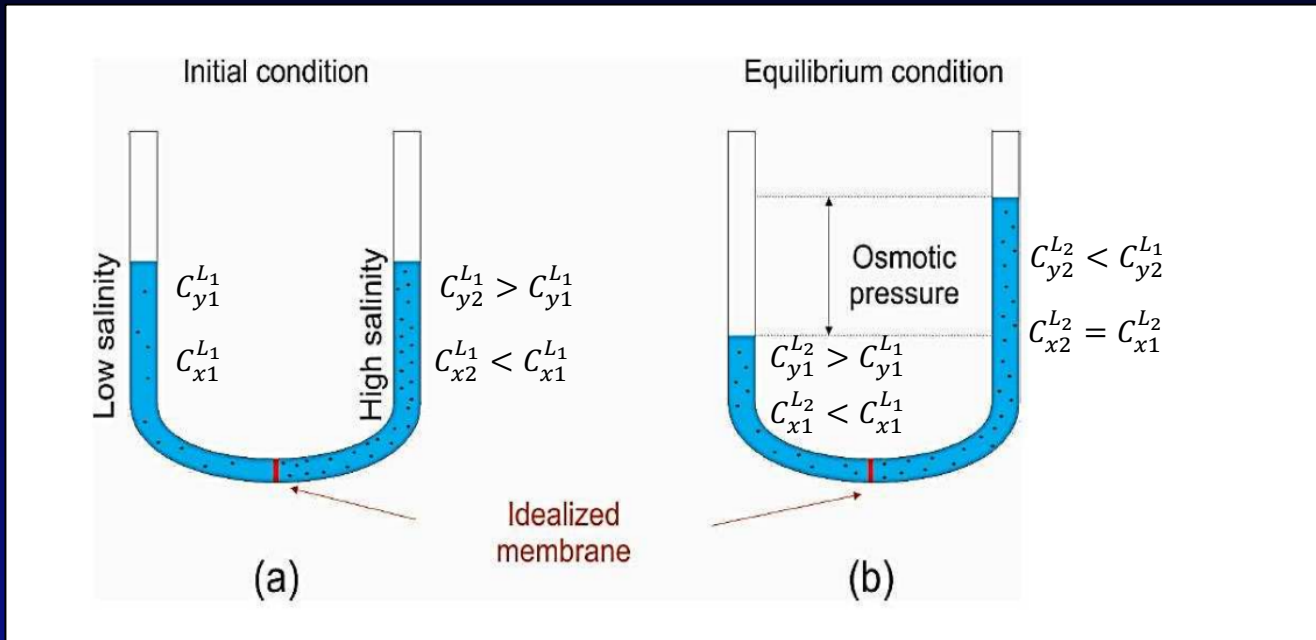
Selective passage of components



[Han 2008]

Hindered Transport

Osmosis

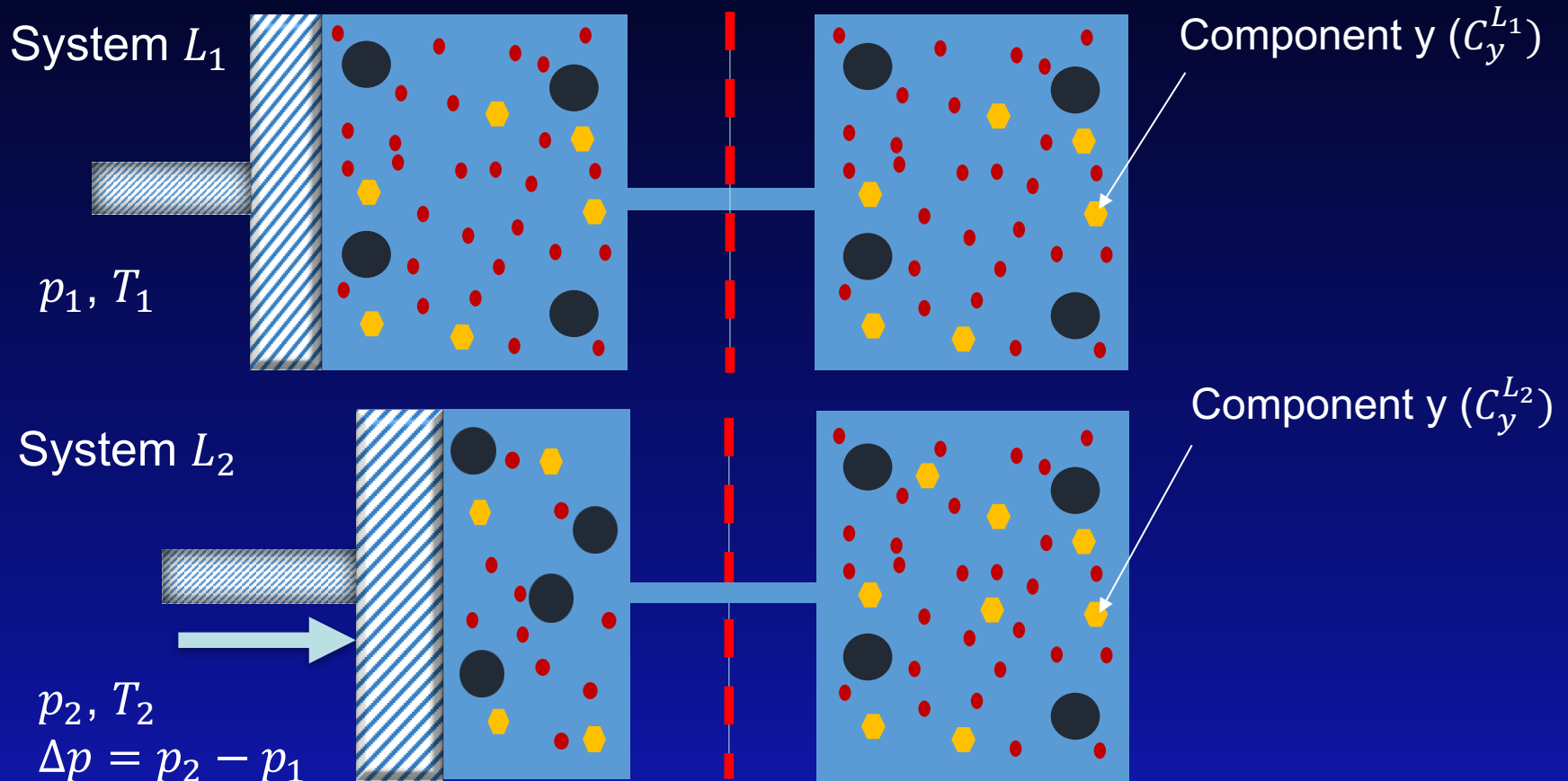


Partition Coefficient $\Phi = \Delta C_y / C_{y2}^{L1}$ $\Delta C_y = C_{y2}^{L1} - C_{y2}^{L2}$

Osmotic Efficiency (reflection coefficient) $\sigma_o = (1 - \Phi)^2$

Hindered Transport

Partition Coefficient, $\Phi = \Delta C_y / C_y^{L_1}$ $\Delta C_y = C_y^{L_2} - C_y^{L_1}$



Φ depends on p & T

Hindered Transport

Volume and Solute Fluxes across a Semipermeable Membrane

Volume Flux: $J_v = L_p(\Delta p_\infty - \sigma_o \Delta \Pi_\infty)$

Solute Flux : $J_s = \omega \Delta \Pi_\infty + (1 - \sigma_f) C_\infty J_v$

Δp_∞ : hydraulic pressure gradient (unhindered)

$\Delta \Pi_\infty$: osmotic pressure gradient ($\Delta \Pi_\infty = RT \Delta C_\infty$, unhindered)

L_p : hydraulic permeability [$L_p = \gamma r_o^2 / (8 \mu L)$]

ω : permeation coefficient [$\omega = (J_s / \Delta \Pi_\infty)_{J_v=0}$]

σ_o : osmotic reflection (rejection) coefficient [$\sigma_o = (\Delta p_\infty / \Delta \Pi_\infty)_{J_v=0}$]

σ_f : filtration reflection coefficient $\{\sigma_f = 1 - [J_s / (C_\infty J_v)]_{\Delta C_\infty=0}\}$

$\sigma_o \approx \sigma_f$ Staverman (1951), Anderson (1981), Levitt (1975)

$$\sigma_o = (1 - \Phi)^2$$

Hindered Transport

Filtration Efficiency

$$\omega_f = (1 - \Phi)^2$$

$$\omega_f = 1 \quad \text{Ideal membrane}$$

$$\omega_f = 0 \quad \text{Non - selective}$$

$$0 < \omega_f < 1 \quad \text{Non - ideal membrane}$$

For solid filtrates of fixed size and geometry

$$\Phi = (1 - \lambda)^2 \quad \longrightarrow \text{independent of } p \text{ \& } T$$

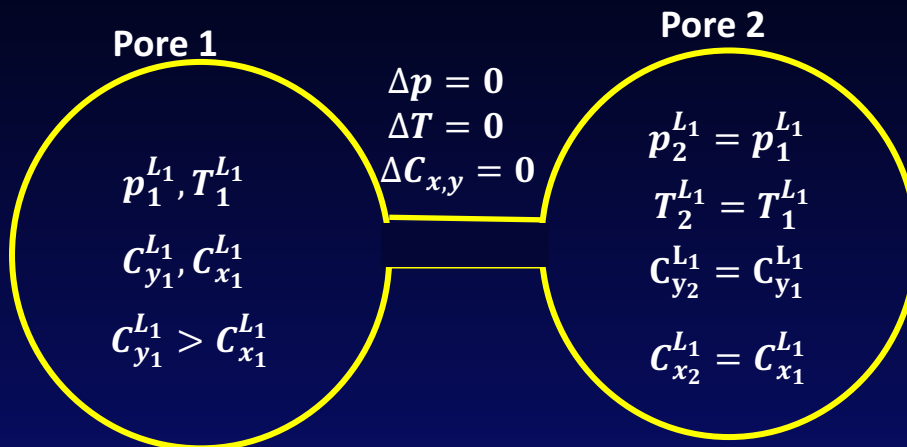
$\lambda = r_s/r_o$: r_s : filtrate particle radius r_o : pore channel radius

For molecular sieving due to steric effects

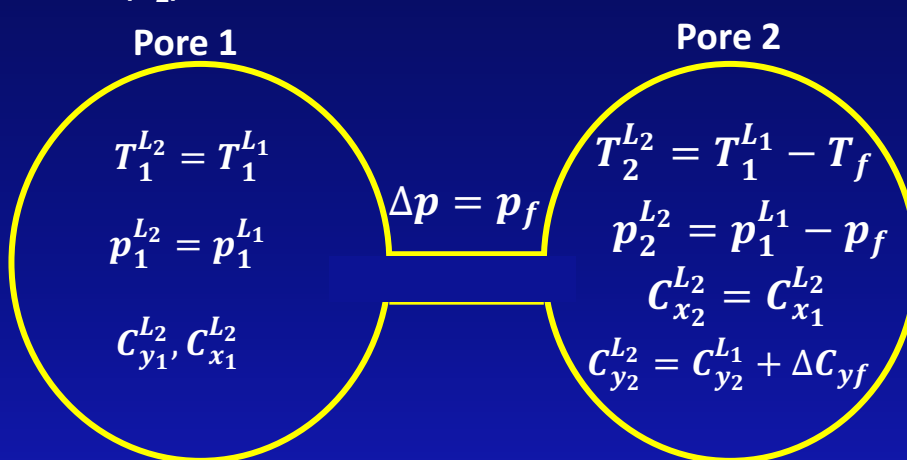
$$\Phi = \Delta C_y / C_y^{L1} \quad \longrightarrow \text{function of } p \text{ \& } T$$

Methodology

System 1 (L_1)



System 2 (L_2)



- Perform flash calculations

- Filtration parameters

$$p_f \equiv \Delta \Pi = p_1^{L_2} - p_2^{L_2} = \Delta p$$

$$T_f = T_1^{L_2} - T_2^{L_2} = \Delta T$$

- Compute fugacities

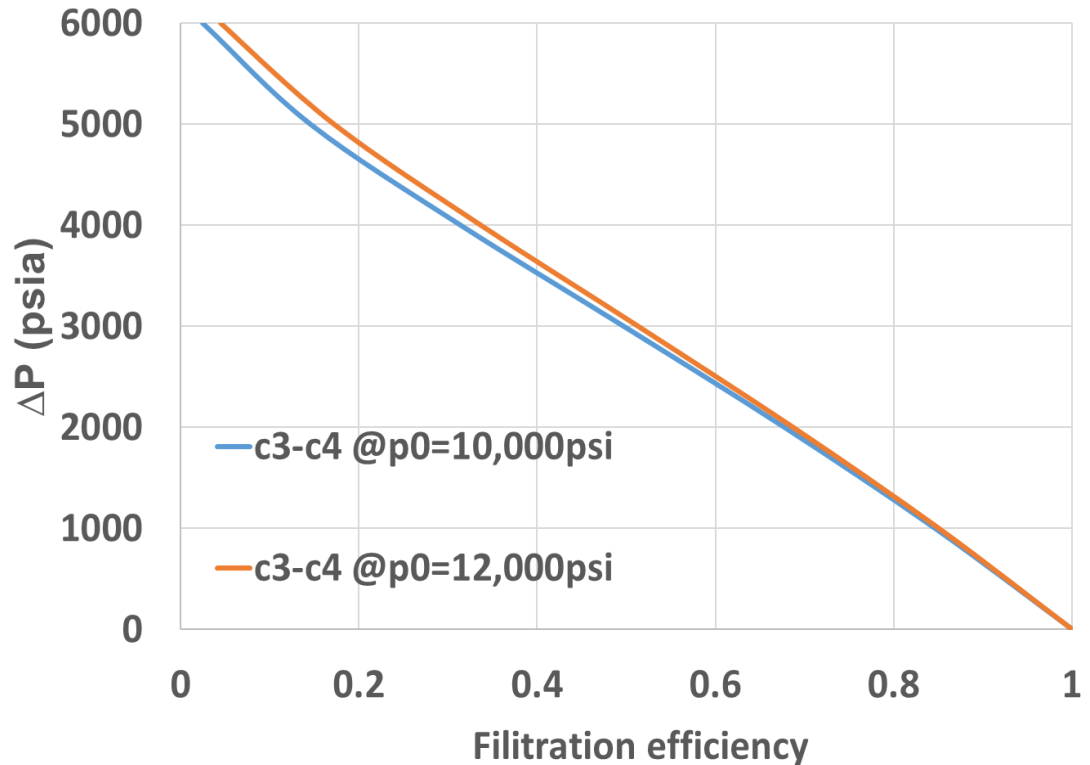
$$f_{C_x}^{L_1} = f_{C_x}^{L_2} \quad f_{C_{y_2}}^{L_2} \neq f_{C_{y_1}}^{L_2}$$

- Compute filtration efficiency

Results

Case 1:

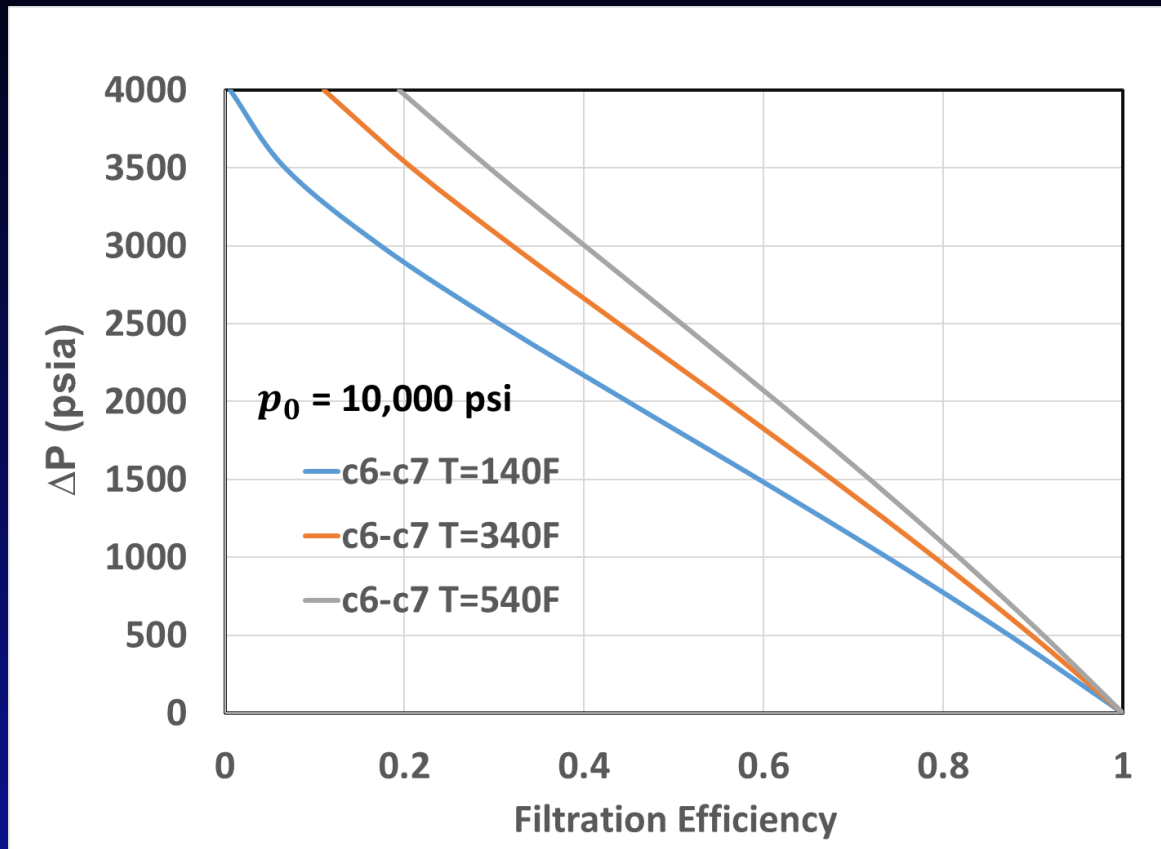
- 2 Components
- Mole fraction:
30% 70%
- Constant temperature:
200 °F
- Pressure change:
0 psi-4000 psi



Results

Case 2:

- 2 Components
- Mole fraction:
30% 70%
- Temperature:
140°F, 340 °F, 540 °F
- Pressure change:
0 psi-4000 psi

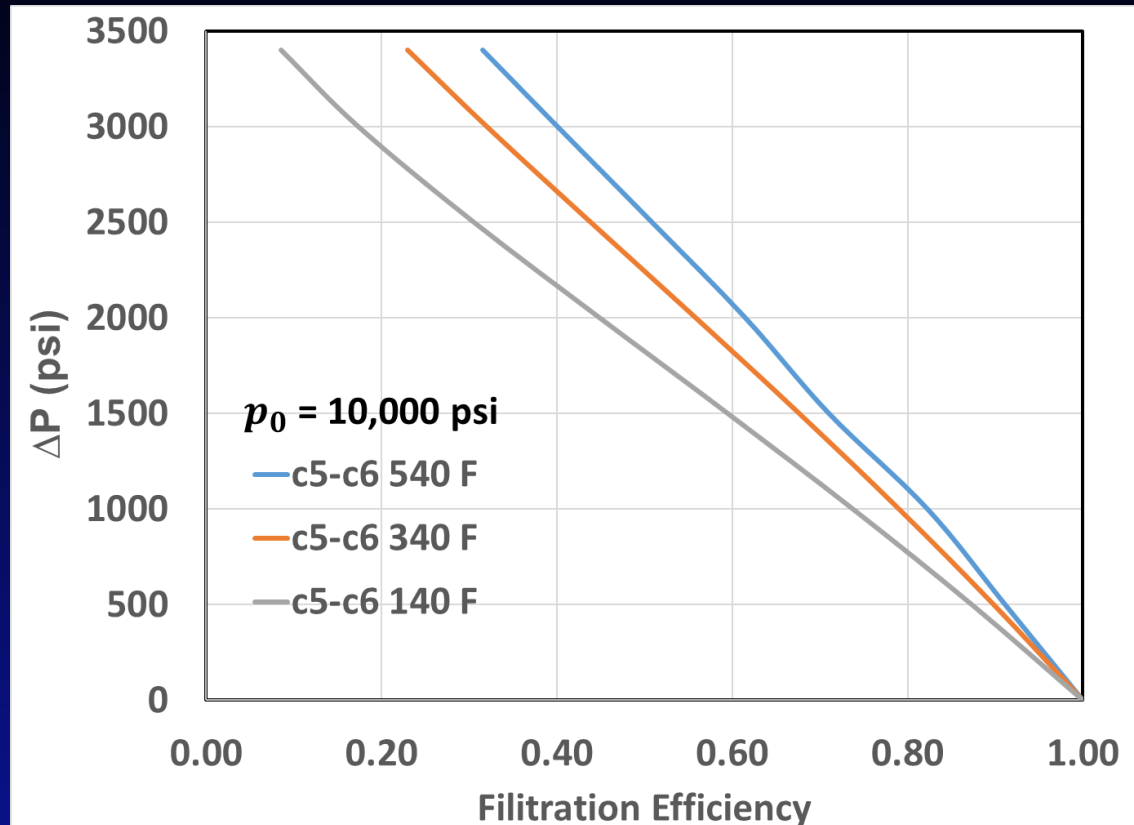


May create a stimulation effect

Results

Case 3:

- 2 Components
- Mole fraction:
30% 70%
- Temperature:
140°F, 340 °F, 540 °F
- Pressure change:
0 psi-4000 psi

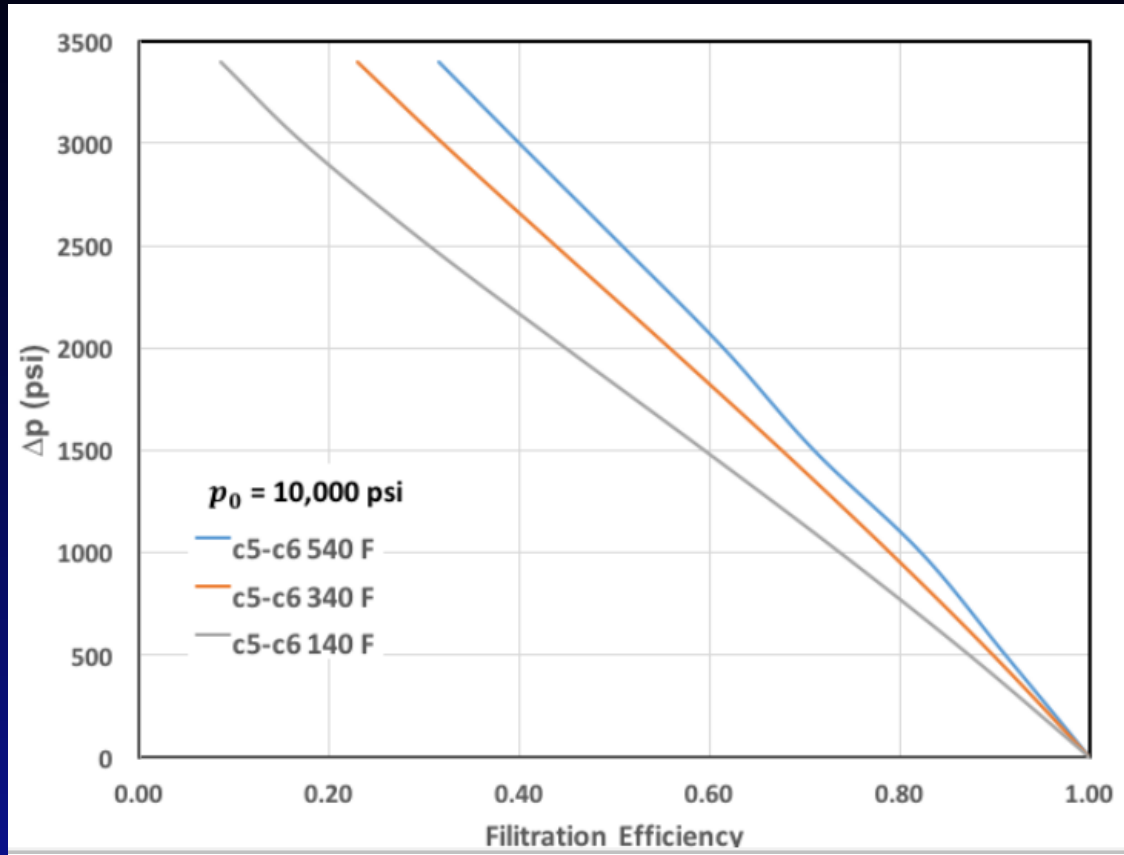


Results

Case 4:

Continuous Change of Composition

- 2 Components
- Mole fraction:
30% 70%
- Temperature:
540°F
- Pressure change:
0 psi-4000 psi



Conclusions

- Filtration efficiency of the medium decreases with increasing pressure and temperature
- Heavier components have lower filtration efficiency at lower temperatures
- For a given filtration pressure, cooling porous medium reduces the filtration efficiency and increases the passage of the heavier components
- Because lighter hydrocarbons are produced during early production, cooling the vicinity of the wellbore may increase the recovery of heavier components
- Model can be applied to multicomponent mixtures by pseudo component grouping

Future Works

- Extend calculations to filtration in a multi-cell system representing a porous medium with varying pore sizes
- Develop a compositional model based on the fluxes for the hindered and unhindered components
- Include water phase in the system and incorporate the steric hindrance of solid particles (salt) and osmotic flows in the model

Thank you!