



**UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT**  
Colorado School of Mines



## Research Summary

# Modeling Fluid Transfer from Shale Matrix to Fracture Network

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**UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT**

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# Problem Statement - A

## Suggested Study - A

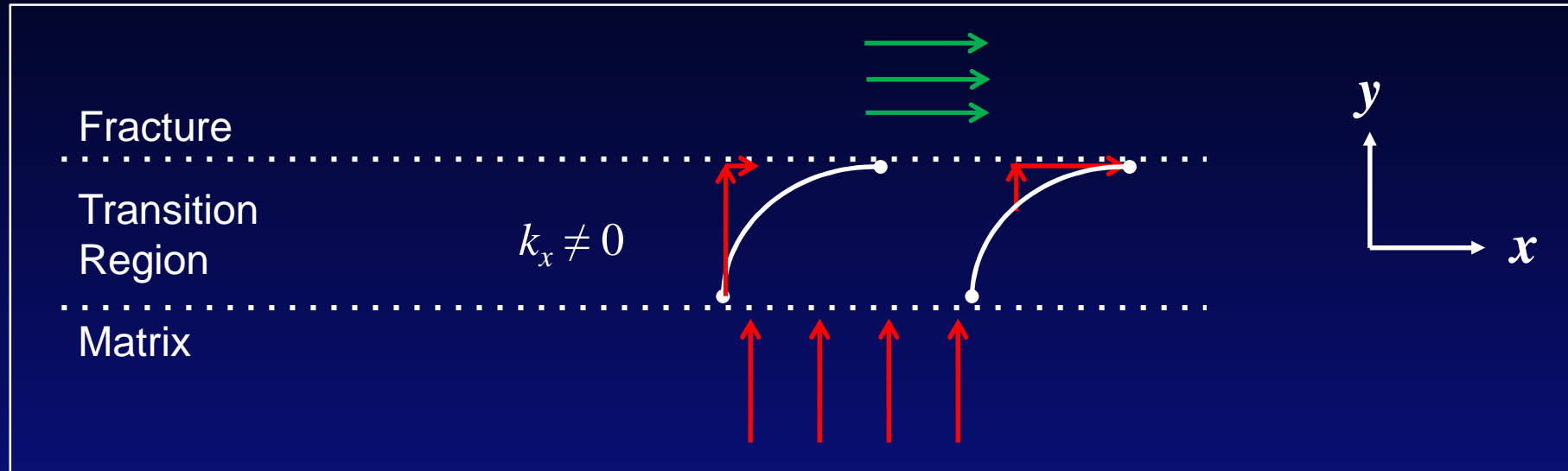


Figure 1: Investigated Behavior for Flow From Matrix to Fracture

- We are interested in investigating the possible contribution of the tangential velocity component ( $v_x$ ) to the mass flux going into the fracture (drag forces).



# Scope of Study - A

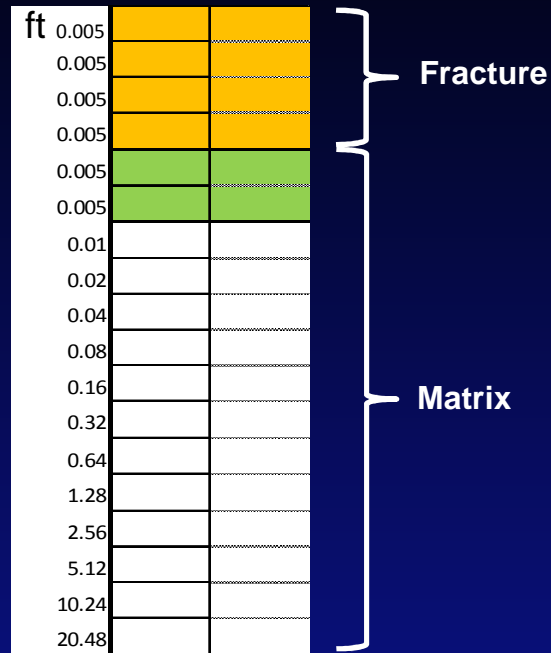


Figure 2: Conventional Modeling

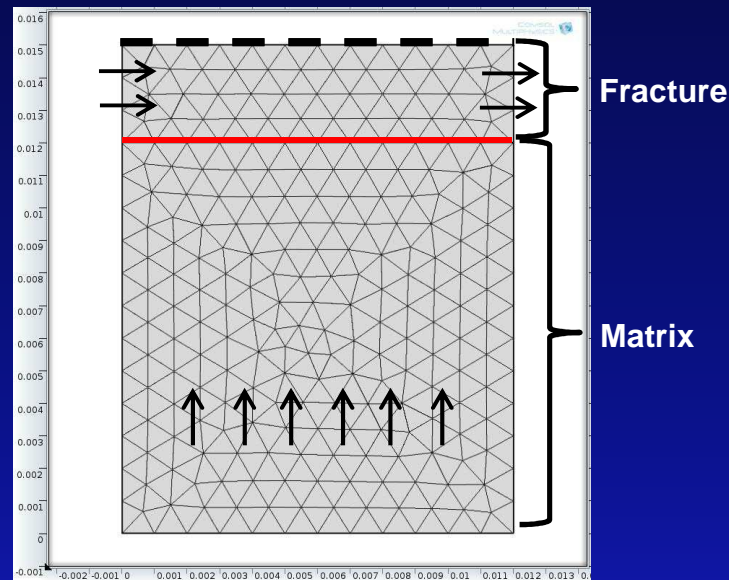


Figure 3: Modeling with COMSOL

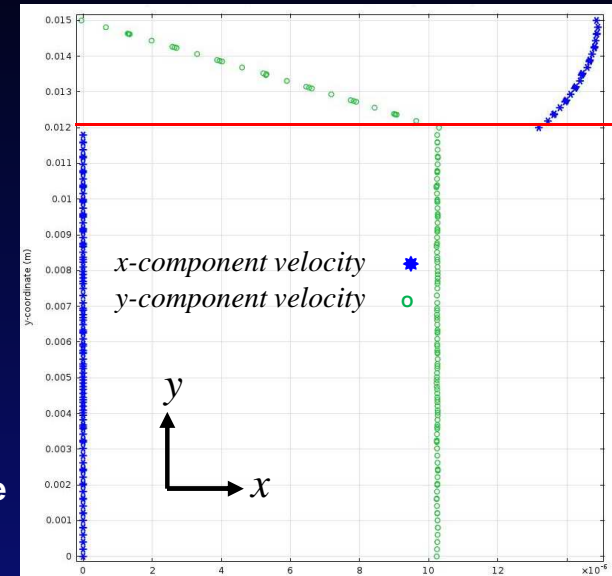


Figure 4: COMSOL Results

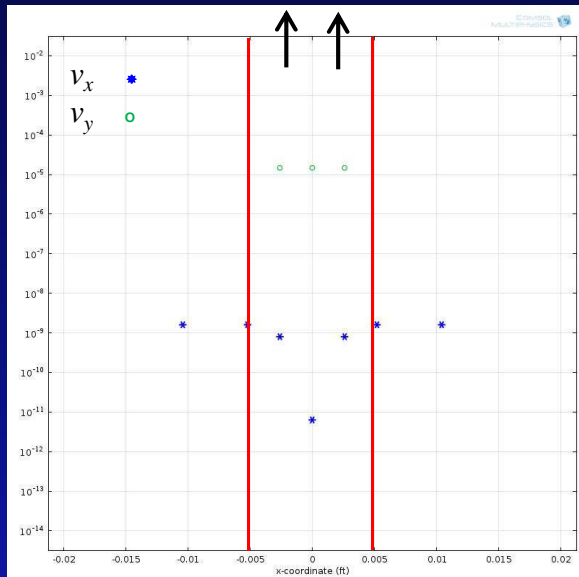


# Results Review - A

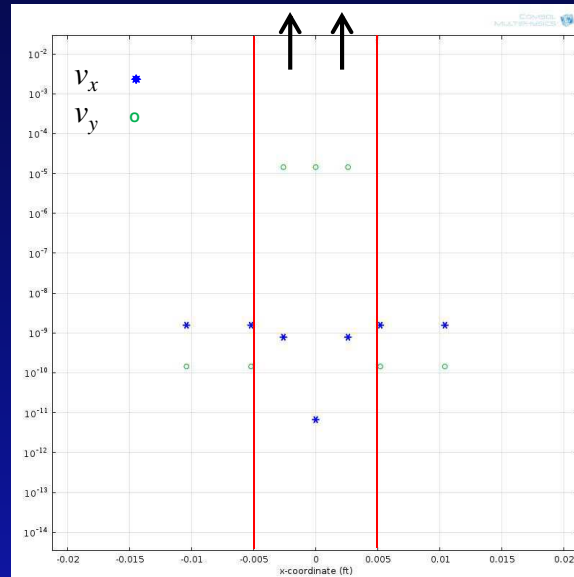
- Results are **dependant** on  $(w_f/h_m)$ ,  $(k_f/k_m)$ ,  $x_f$  and boundary conditions (pressure, slip/no-slip wall).

Table 1: Sample Sensitivity Range

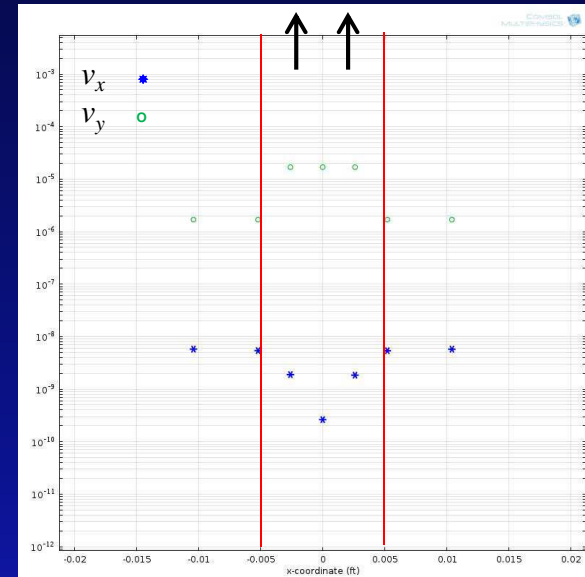
$w_f/h_m$	$k_f/k_m$
1:1	10
1:2	100
1:4	1,000
1:10	10,000



a) No Tangential Contribution



b) Suggested Study  $k_f/k_m = 100$



c) Suggested Study  $k_f/k_m = 10,000$

Figure 5: COMSOL Results for  $k_f/k_m$  Sensitivity



# Results Review - A

- Research is ongoing, we are trying to find a more accurate/detailed methods/equations and better setup of the problem.
- Is it possible to generalize the results in the form of a conventional transfer function?



# Problem Statement - B

- Multi-stage hydraulic fracturing (HF) is necessary for unconventional wells to be economical.
- HF can increase the permeability of naturally fractured reservoirs by opening pre-existing closed fractures (shear dilation and fluid leak-off).
- Stimulated Reservoir Volume (SRV) is assumed to have uniform properties ( $k_{nf}$  and  $\rho_f$ ).



# Problem Statement - B

- How **accurate** are the models representing the SRV in terms of average natural-fracture properties ( $k_{nf}$ ,  $\rho_f$ , etc.)?

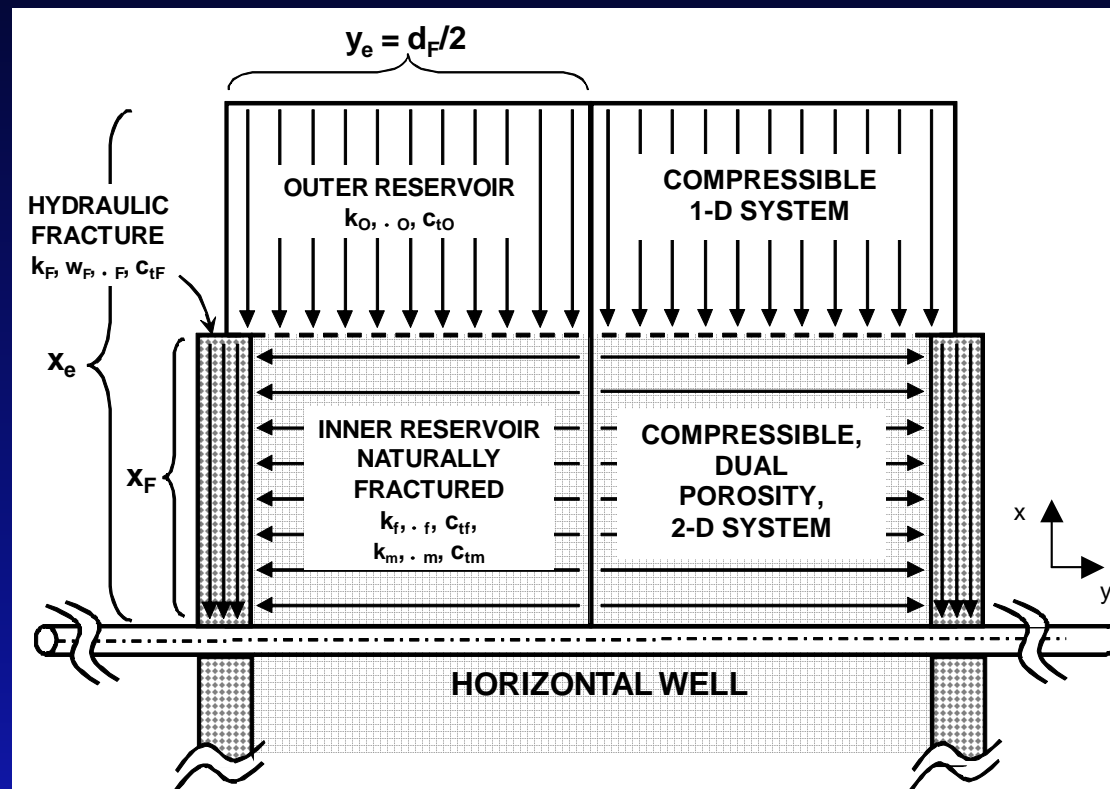


Figure 6: Tri-linear Flow Model (Ozkan et al., 2009)



# Problem Statement - B

- Induced stress is maximum near HF → increased microseismic events are observed.
- As we move further from HF  $k_{nf}$  and  $\rho_f$  will decrease.

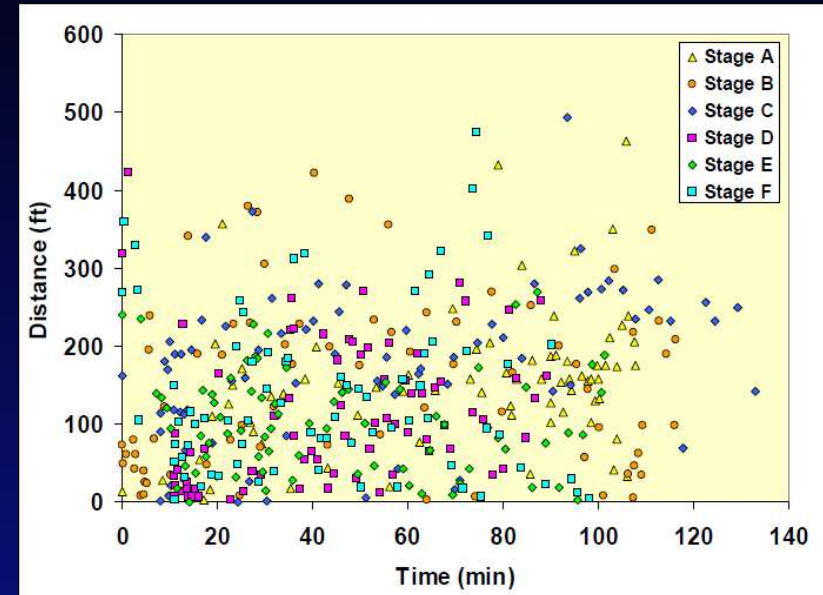


Figure 7: Microseismic Events for Horizontal Well with Multi-stage Hydraulic Fracturing (Warpinski 2009)





# Scope of Study - B

- Derive an analytical solution assuming a linear composite SRV between hydraulic fractures.

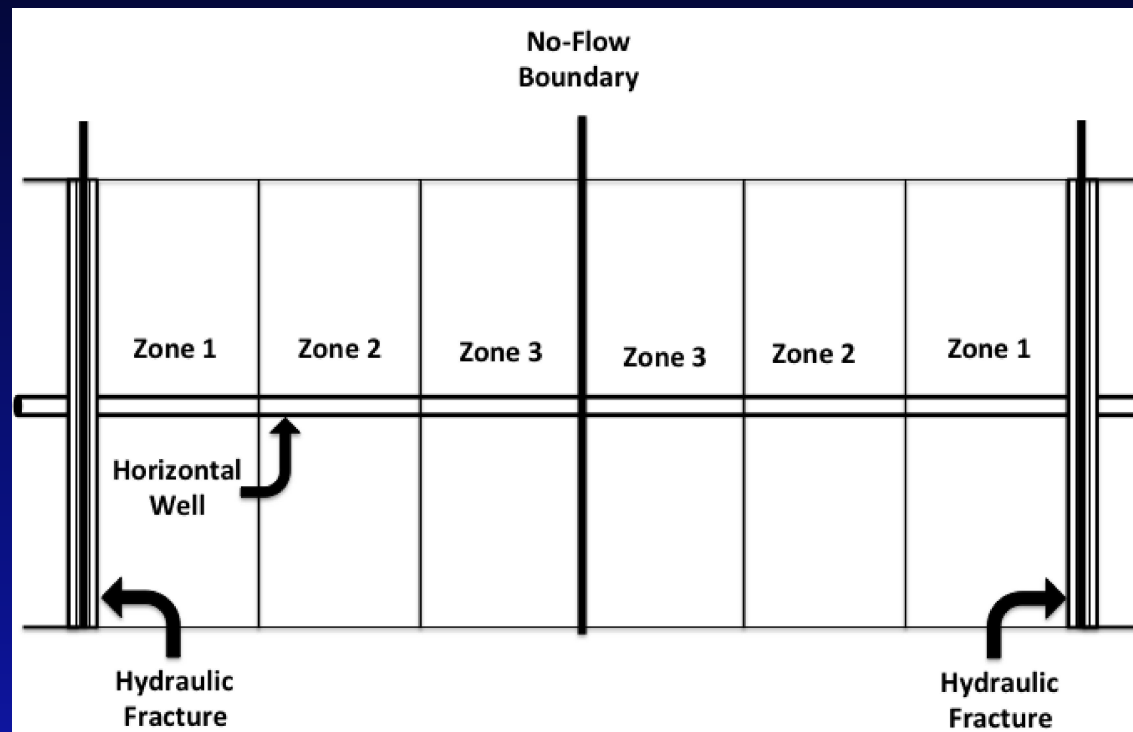


Figure 8: Example of Composite SRV



# Scope of Study - B

- Compare the production responses obtained from the linear-composite and “homogenous” SRV models:
  - Is homogenous SRV assumption valid?
  - What are the limitations?
  - Are there any diagnostic features of production data indicating composite SRV?
  - Can the results be generalized for continuously changing natural fracture properties away from the hydraulic fracture?



# Analytical Modeling - B

- Identical fractures uniformly distributed along the well.
- Model the region between two hydraulic fractures.
- Tri-zone linear composite SRV between fractures.
- No-flow beyond SRV.

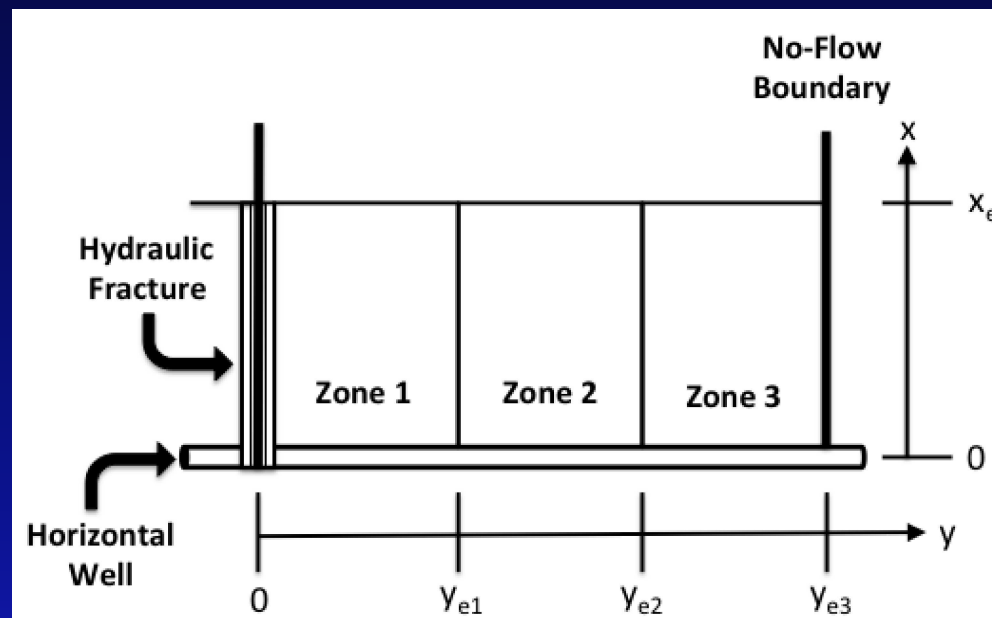


Figure 9: Tri-zone Composite SRV



# Analytical Modeling - B

Solution:

$$\bar{p}_{wD} = \frac{\pi}{s C_{FD} \sqrt{\alpha_F} \tanh\left(\sqrt{\alpha_F}\right)}$$

$$\alpha_F = \frac{2\beta_F}{C_{FD}} + \frac{s}{\eta_{FD}}$$

$$C_{FD} = \frac{k_F w_F}{k_r x_F} \quad \eta_{FD} = \frac{\eta_F}{\eta_r} \quad \eta = \frac{k}{\phi c_t \mu}$$



# Analytical Modeling - B

Solution (Continued):

$$\beta_F = \sqrt{s_1} \frac{\sinh \left[ \sqrt{s_1} \left( y_{e1D} - \frac{w_D}{2} \right) \right]}{\cosh \left[ \sqrt{s_1} \left( y_{e1D} - \frac{w_D}{2} \right) \right] - \frac{\Omega}{2(1+\Omega)}}$$

$$\Omega = \frac{\sqrt{\eta_1}}{\sqrt{\eta_2}} \left\{ \frac{\tanh \left[ \sqrt{s_2} (y_{e1D} - y_{e2D}) \right]}{\exp \left[ \sqrt{s_1} (y_{e1D} - y_D) \right]} \right\}$$

$$\times \left\{ 1 + \left( \frac{k_3 \sqrt{\eta_2}}{k_2 \sqrt{\eta_3} + k_3 \sqrt{\eta_2}} \right) \frac{\exp \left[ -\sqrt{s_2} (y_{e1D} - y_{e2D}) \right]}{\left\{ 1 - \cosh \left[ \sqrt{s_2} (y_{e1D} - y_{e2D}) \right] \right\}} \right\}$$

$$s_i = \frac{s}{(\eta_i / \eta_r)}$$



# Work to be done - B

## Solution (Continued):

- Solution defaults back to the “homogeneous” SRV solution for uniform properties (or single zone).
- Computational code is being developed.
- The next step is to derive a general solution for n-zone linear-composite SRV model.



# Thank you

