

#### UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT Colorado School of Mines

CS

#### Thermodynamics of Multiphase Flow in Unconventional Liquids-Rich Reservoirs

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## **Classical Thermodynamics**

- Industry norm is to use EOS or PVT tables
- PVT behavior from PVT cells ignoring
  - capillary pressure
  - surface forces



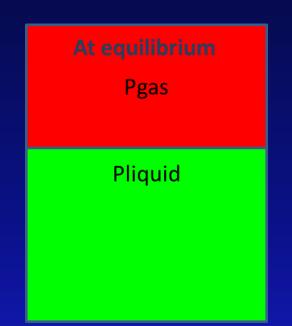
UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT Kick-Off Meeting, November 16, 2012, Golden, Colorado



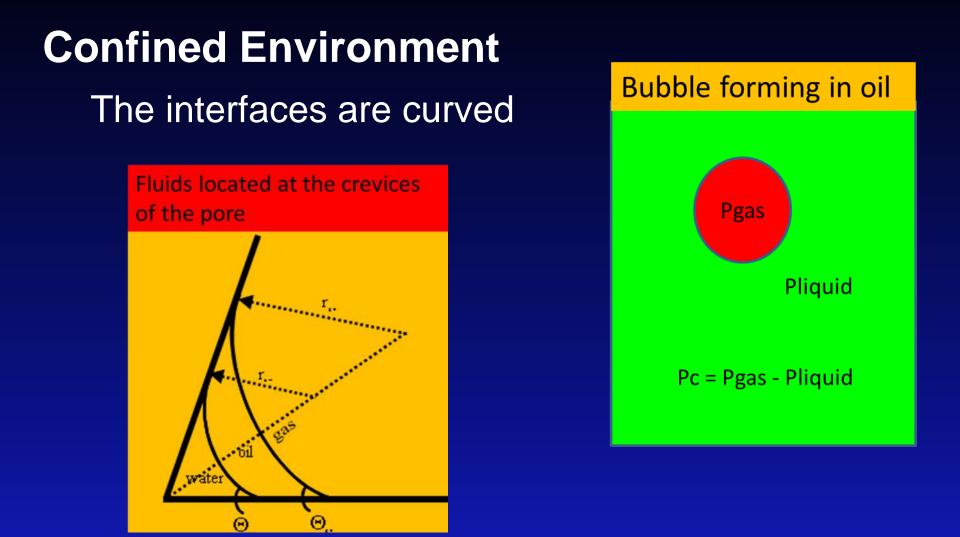
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## **Classical Thermodynamics**

#### Gas phase appears at bubble-point pressure





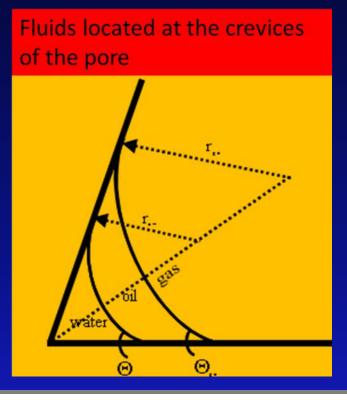




## **Confined Environment**

## Capillary forces, surface forces

should not be neglected

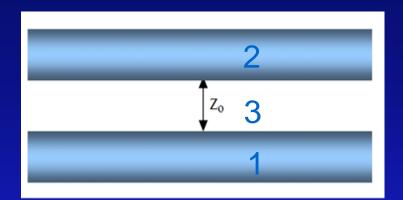




**Capillary Pressure (Laplace Equation)** 

$$P_g - P_L = \frac{2\sigma}{r}$$

#### Addition of surface forces



$$P_G - P_L = \frac{2\sigma}{R} + \Pi$$
$$\Pi = -\frac{A_{132}}{6\pi z_o^3}$$



## **Confined Environment**

• Extra energy cost due to these forces should be included in phase behavior calculations

• Small pores – impact can be significant



## Phase Equilibrium is reached at different liquid and gas pressures

Altered VLE

Altered bubble point pressure



# In this study the impact of confinement manifests itself as:

- reduction (suppression) of the saturation pressure
- changes in the gas composition at the bubble point

## extension of the Bo curve



PR EOS was used for solution

EOS parameters for the fluid samples were determined through regression to lab measurements



Since P<sub>I</sub> and P<sub>g</sub> are not equal,

VLE was solved for two pressures for the two phases

K value definition is modified and  $\mathrm{K}_{\mathrm{c}}$  definition is used



#### Approach

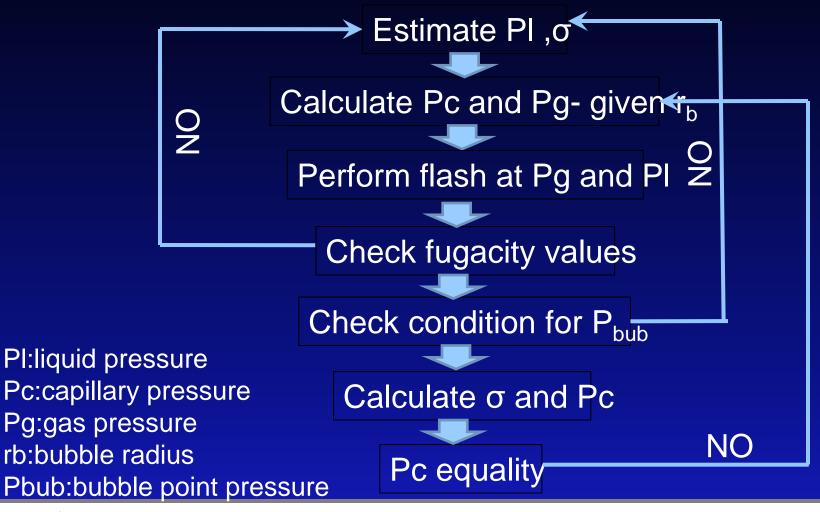
$$K_{ci} = K_i \frac{p_l}{p_g}$$

#### where

$$K_{i} = \frac{\left[\frac{f_{i}^{L}}{x_{i}P_{l}}\right]}{\left[\frac{f_{i}^{v}}{y_{i}P_{g}}\right]} = \frac{\varphi_{i}^{L}}{\varphi_{i}^{v}}$$



#### Approach





## Application to three samples from unconventional reservoirs

Sample 1: Monterey Sample 2: Bakken Sample 3: Eagle Ford



### **Impact of Surface Forces**

$$P_G - P_L = \frac{2\sigma}{R} + \Pi$$
$$\Pi = -\frac{A_{132}}{6\pi z_o^3}$$

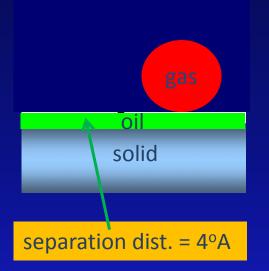
Hamaker constant (A) is a function of refractive indexes and dielectric constants of the fluids and the surfaces involved

## Literature values of oil, gas and dolomite were used in calculations

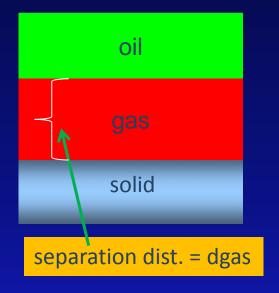


## **Impact of Surface Forces**

#### Particle close to a surface

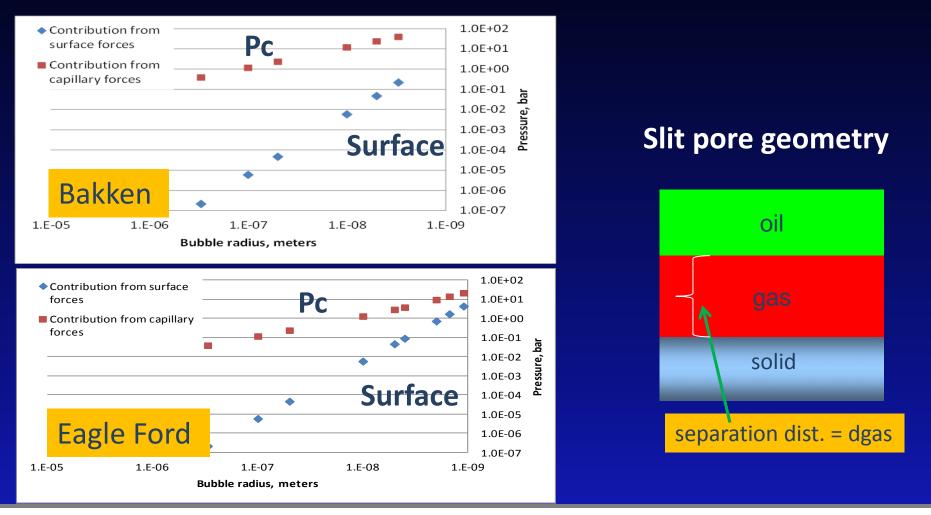


#### Slit pore geometry





## **Impact of Surface Forces**

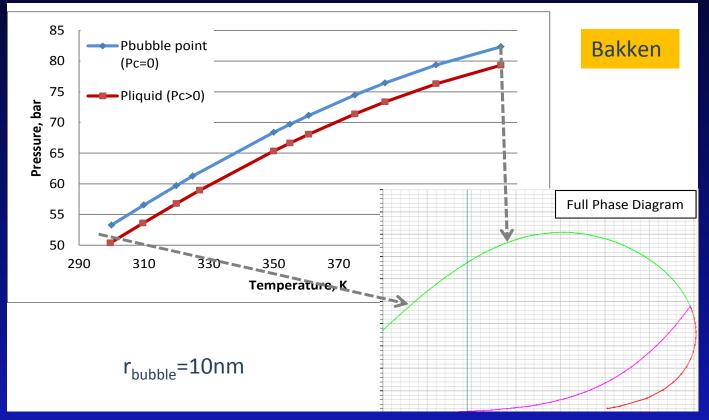




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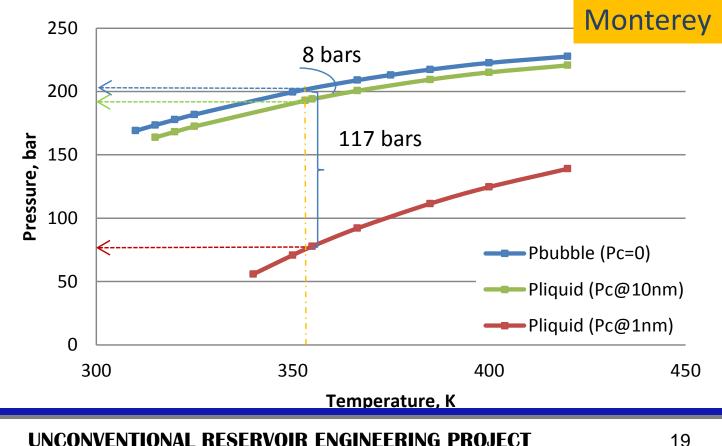
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# Phase Diagram Shift and Bubble Point Suppression



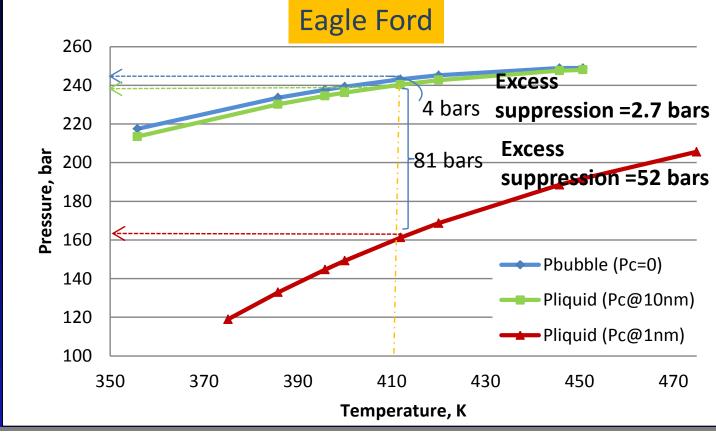


## Phase Diagram Shift and Bubble Point **Suppression**



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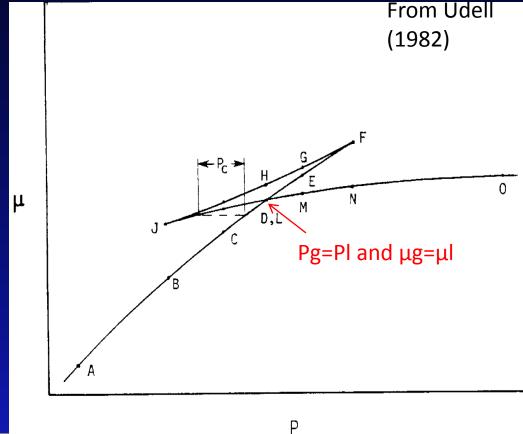
## Phase Diagram Shift and Bubble Point Suppression





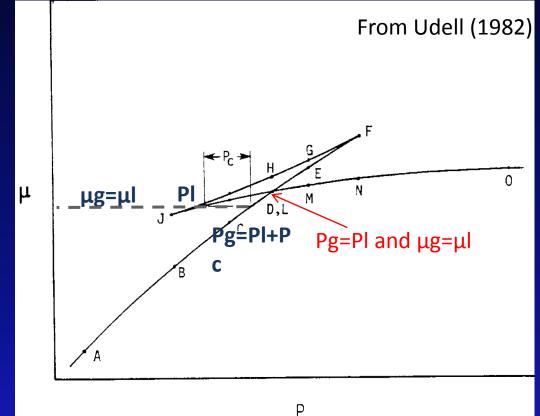
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# Phase Diagram Shift and Bubble Point Suppression



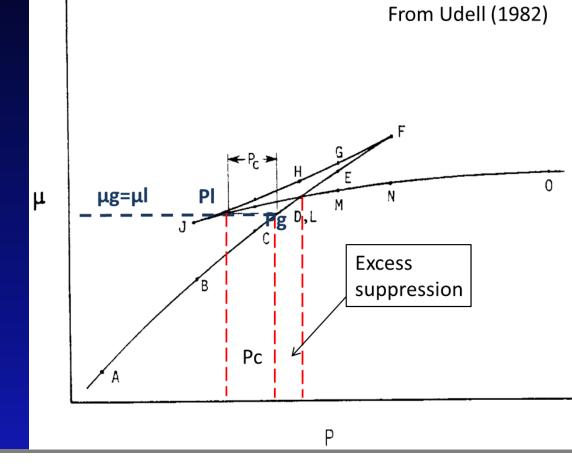


# Phase Diagram Shift and Bubble Point Suppression



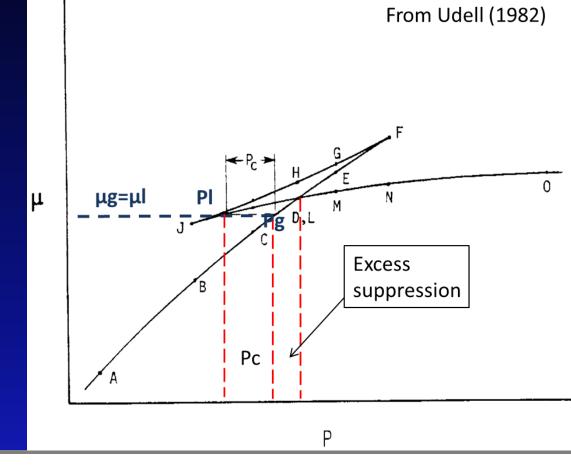


## Phase Diagram Shift and Bubble Point Suppression





## Phase Diagram Shift and Bubble Point Suppression



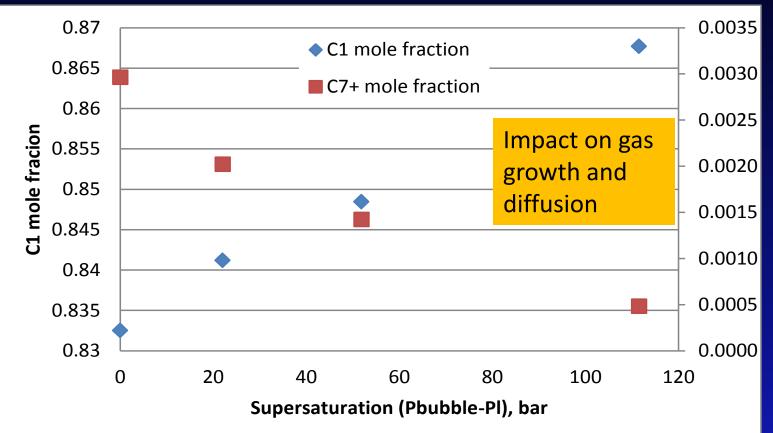


# Gas Composition Change due to Suppression

The gaseous phase contains lighter components as the bubble-point suppression increases.



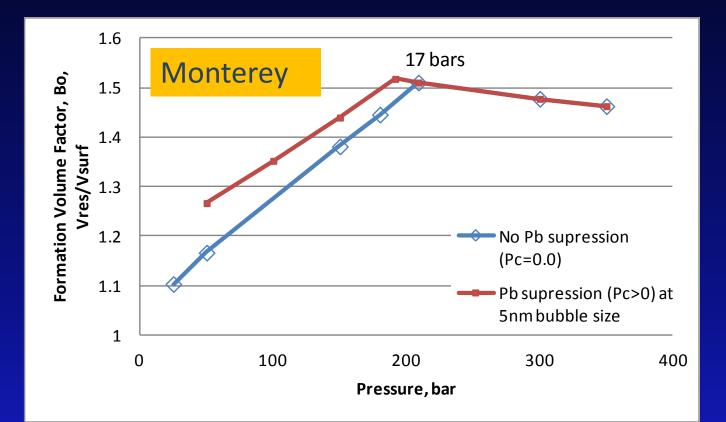
The gaseous phase contains lighter components as the bubble-point suppression increases.





## **Formation Volume Factor**

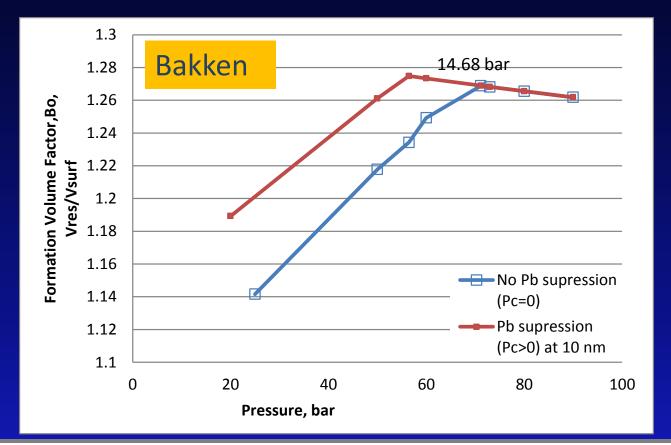
Undersaturated portion of the curve is extended





## **Formation Volume Factor**

Undersaturated portion of the curve is extended





Oil Volume in Equilibrium with the First Gas Bubble Possible pore sizes...

Common approach is to assume that the gas bubble occupies the entire pore space

 $r_{bubble} = r_{pore}$ 

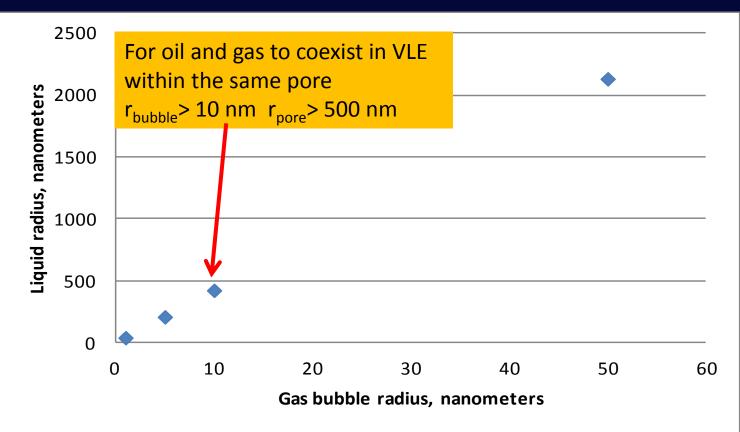


We investigate the gas bubble being in equilibrium with the oil that occupies the rest of the pore

**Assumption:** At bubble point gas bubble is infinitesimal (mole fraction 10<sup>-5</sup>)



## Gas bubble is in equilibrium with the oil that occupies the rest of the pore





#### Conclusions

In confinement the bubble-point pressure is suppressed and the excessive suppression amount is a function of the bubble radius and the interfacial tension.

For the particular examples considered in this paper, the contribution of the surface forces was small. However, the trends indicate the possibility of surface forces becoming significant.



#### Conclusions

The pore size may constraint the gas formation in a confined environment.

Due to suppression equilibrium gas composition will be different .

For a confined fluid, the undersaturated portion of  $B_o$  must be extended to lower pressure values.



## **Future Work**

Verify the impact of confined phase behavior on flow

Develop a **reservoir simulator** that incorporates the findings



**Future Work** 

Black Oil Application

**PVT** tables

Pc



## **Future Work**

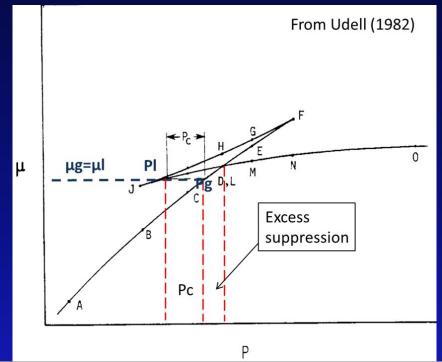
Unconventional simulator should address

PVT property evaluation at different pressures for oil and gas



## **Future Work**

#### Unconventional simulator should address Excess suppression





### **Future Work**

Excess suppression needs to be correlated and input into the simulator

If data is not available it can be handled as a history matching parameter

It may be calculated as a function of bulk Psat (composition @ bulk Psat) and the bubble radius



## **Future Work**

The suppression values increase with the decreasing radius (more confinement)

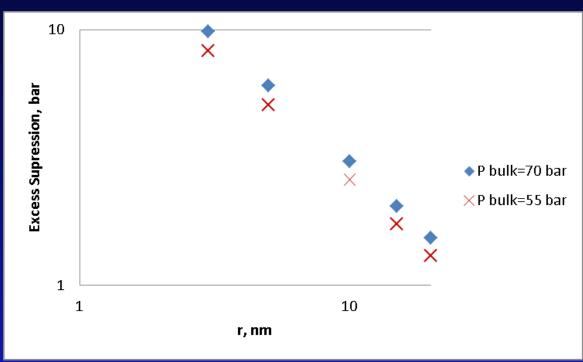
Trends are consistent with bulk pressure within a sample but different for different samples



### **Future Work**

#### Example Trend – low GOR, low pressure

Excess suppression decreases with decreasing pressure

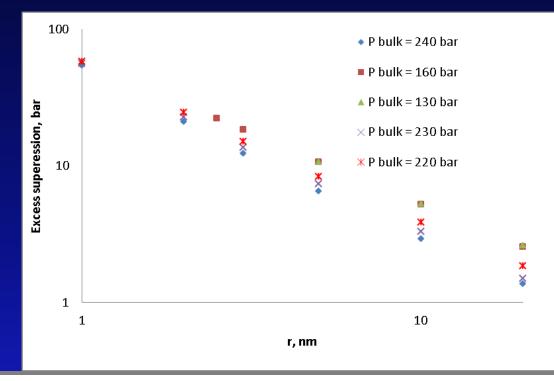




### **Future Work**

#### Example Trend – high GOR, high pressure

Excess suppression increases with decreasing pressure





### **Future Work**

Chet Ozgen will explain how to incorporate these findings into a reservoir simulator



## Thank you!

