

#### **Research Summary**

### **PSEUDOTRANSIENT LINEAR FLOW ANALYSIS**

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**UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT** 

Advisory Board Meeting, May 5, 2017, Golden, Colorado

### **Trilinear Flow Model**



HF: Hydraulic Fracture NF: Natural Fracture IM: Inner Matrix OM: Outer Matrix HW: Horizontal Well



# Trilinear Flow Regimes (FR)

Early times (no contribution from IM) FR 1: HF linear flow FR 2: Early bilinear flow in HF & NF FR 3: Transient linear flow in NF only (no contribution from HF)

Intermediate times (transient contribution from IM) FR 4: Late bilinear flow in NF & IM FR 5: Trilinear flow in HF, NF & IM (highly unlikely) FR 6: Pseudotransient linear flow in NF & IM FR 6A: Transient flow in NF and boundary dominated flow in IM (high λ') FR 6B: Transient flow in IM and boundary-dominated flow in NF (low λ')

Late times (pseudosteady contribution from IM) Boundary dominated flow in NF & IM, no flow from OM Boundary dominated flow in NF & IM, and transient linear flow from OM Boundary dominated flow from HF, NF, IM, & OM



### Flow Regimes 3 & 6



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FR 3: Transient linear flow FR 6: Pseudotransient linear flow

Condition for FR 6 (pseudotransient linear flow) Dual-porosity slab configuration May be too idealized for naturally fractured media

May be applicable in layered systems (dual-permeability)





Producing layer (fractured carbonate)

Eagle Ford, Bakken?



### Flow Regimes 3 & 6





#### Log-log diagnostic plot



Identify linear flow trend and mark up the start and end times



#### Cartesian (square-root-of-time) plot



Assume FR 6B

Use the equations for the slope of the straight line and the start & end of linear flow to obtain matrix properties,  $k_m$ and  $(\phi c)_m$ .







If fracture properties are known, match data with model for verification Else, use matrix properties in regression to obtain fracture properties Check the

Check the existence condition of FR 6B for consistency



#### Equations used in the analysis

$$k_{m} = \left[\frac{0.7980\mu h_{m}}{m n_{F} x_{F} n_{f} (y_{e} - \frac{W_{F}}{2})\Delta p}\right] \sqrt{\frac{180.13}{t_{e6}}} \quad \text{Slope}$$

$$t_{b6b} = 42,230 \left(y_{e} - \frac{W_{F}}{2}\right)^{*} \frac{\kappa_{m} c_{m} \varphi_{m} \mu}{k_{f}^{2} h_{f}^{2}} \quad \text{Start of FR 6B if it follows bilinear flow}$$

$$t_{b6b} = \frac{1.35 \times 10^{5} \left(y_{e} - \frac{W_{F}}{2}\right)^{2} c_{f} \phi_{f} \mu}{k_{f}} \quad \text{Start of FR 6B if no bilinear flow}$$

$$t_{e6b} = \frac{180.13 h_{m}^{2} c_{m} \phi_{m} \mu}{k_{m}} \quad \text{End of FR 6B}$$

$$\frac{\left(h_{f} c_{f} \phi_{f} + h_{m} c_{m} \phi_{m}\right) k_{f} h_{f}}{k_{m} c_{m} \phi_{m} \left(y_{e} - \frac{W_{F}}{2}\right)^{2}} > 4 \quad \text{Existence condition of FR 6B}$$



#### Log-log diagnostic plot



Identify linear flow trend and mark up the end time (start time is not clear)



#### Cartesian (square-root-of-time) plot



Assume FR 3 Use the equations for the slope of the straight line and the end of linear flow to obtain fracture properties, k<sub>f</sub> and  $(\phi C)_{f}$ Verify the existence condition of FR 3



#### Cartesian (square-root-of-time) plot



Repeat the analysis assuming FR 6A & FR 6B

FR 6A: Estimate matrix properties,  $k_m$  and  $(\phi c)_m$ FR 6B: Estimate fracture properties,  $k_f$  and  $(\phi c)_f$ 

Verify the existence of FR 6A & FR 6B (existence of FR 6A is not verified)



#### Model match of the data



Using the data obtained from all three analyses, match the data with the model

Only FR 3 yields an acceptable match



## Conclusions

In unconventional plays where producing layers are interbedded by tight storage layers (shale), pseudotransient linear flow may develop at intermediate times

It is essential to distinguish between transient (FR 3) and pseudotransient (FR 6) linear flows for the accuracy of the analysis

Analysis procedure outlined in this presentation helps identify the correct linear flow and consistently analyze the data

Further details are provided in the PhD dissertation of Wisam Assiri (2017)

