



**UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT**  
**COLORADO SCHOOL OF MINES**



## Research Report

# Investigation of the Interface Conditions Between Nano-Porous Matrix and Fractures of Unconventional Reservoirs

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**UNCONVENTIONAL RESERVOIR ENGINEERING PROJECT**

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# Problem Statement

- Fluid flow from matrix to fractures is commonly addressed by two models:
  - Kazemi de Swaan-O (Transient).
  - Warren-Root (pseudo-steady state).

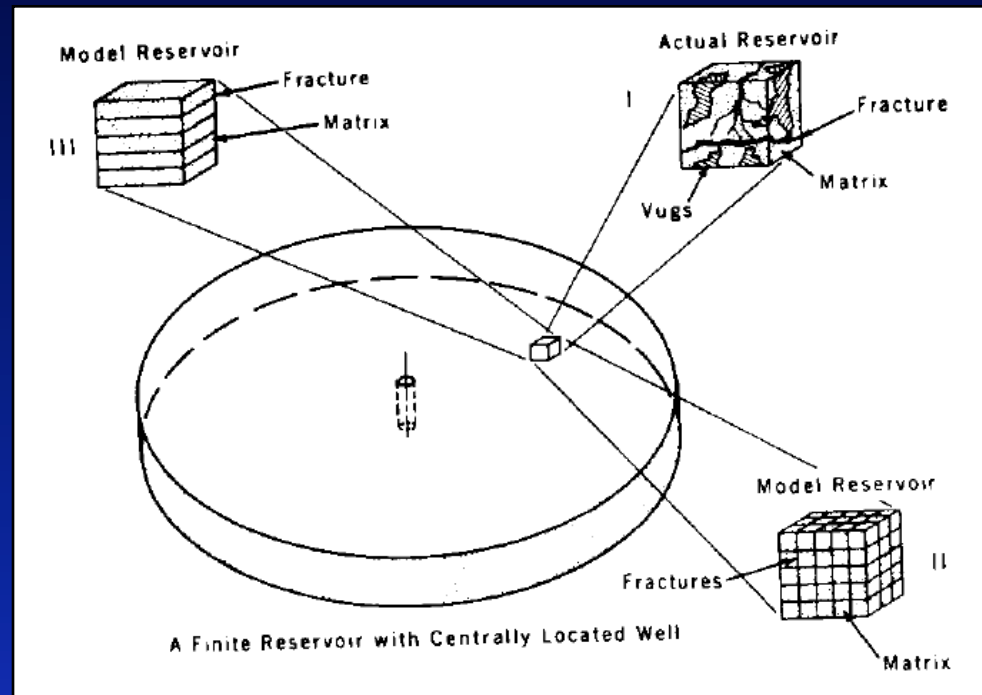


Figure 1: Dual Porosity Idealizations (Kazemi 1969)



# Problem Statement

- Transient model is more suitable for tight matrix. One dimensional flow for both regions.

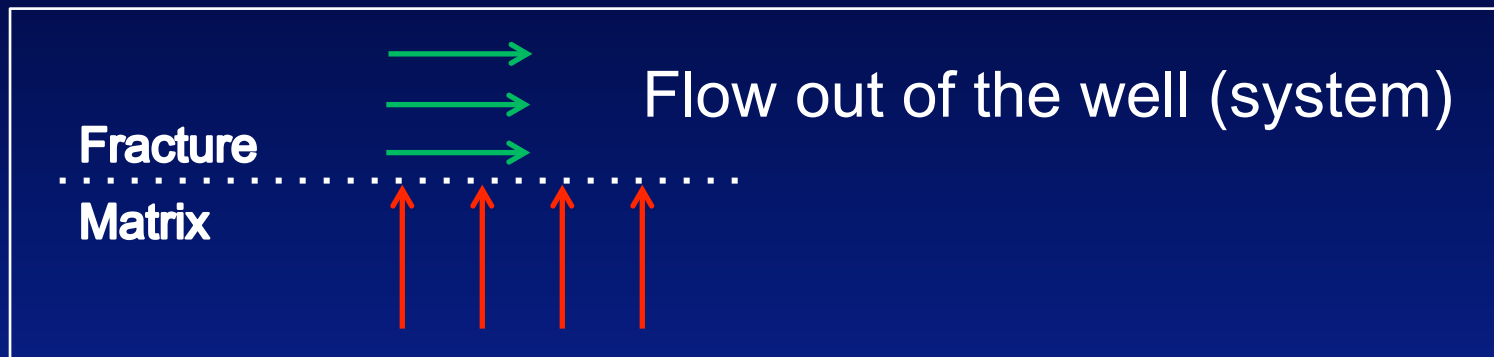


Figure 2: Flow From Matrix to Fracture in Transient Models

- PSS model is zero-dimensional (no matrix shape is required) and does not include the details (direction) of flow from matrix to fracture (matrix provide storage, fracture = provide conductivity).



# Problem Statement

- We are interested in investigating the possible contribution of the tangential velocity component ( $v_x$ ) to the mass flux going into the fracture (drag forces).

## Suggested Study

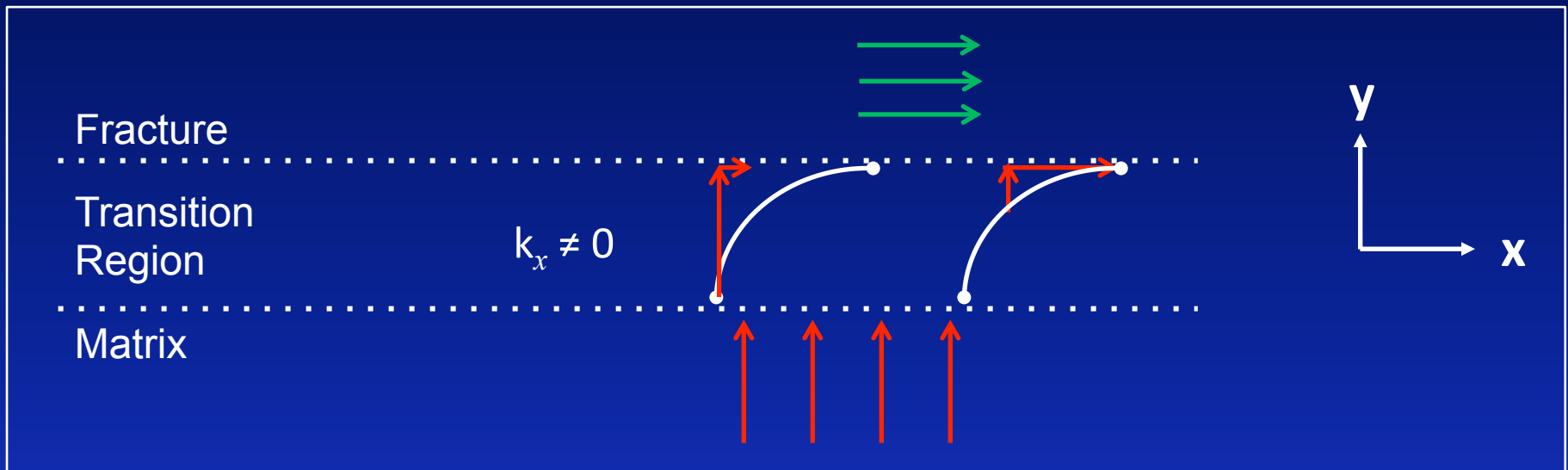


Figure 3: Investigated Behavior for Flow From Matrix to Fracture



# Objectives

- Investigate the details of matrix-to-fracture fluid transfer
- Investigate the effect of large velocity contrast between fracture and matrix media
- Demonstrate the effects of confinement on matrix side
- Extend the results to multi-phase flow
- Define a methodology to incorporate the results to large-scale flow models



# Importance

- Beavers & Joseph 1967.
- Le Bars and Worster 2006.

You may include some explanation for these references

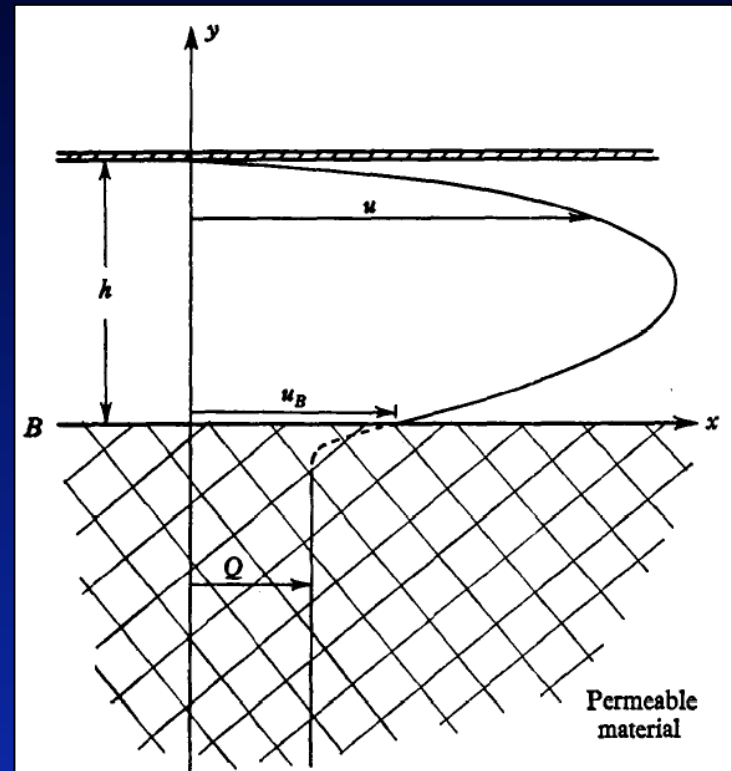


Figure 4: Linear Flow Velocity Profile  
(Beavers & Joseph 1967)



# Importance

- We are looking at the **sharp contrast** in velocities and proper coupling conditions are necessary (Poiseuille-Darcy or Brinkman-Darcy).

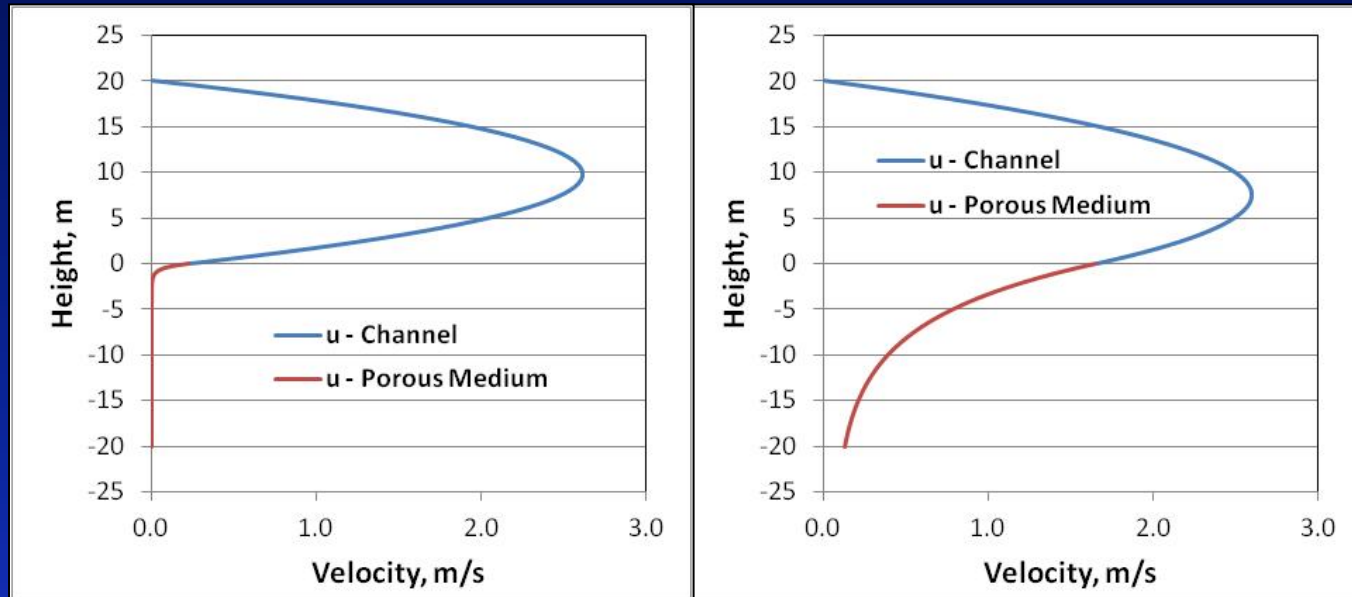


Figure 5: Velocity Profile Under Different Conditions



# Importance

- Modeling using LBM and DEM (paper submitted for the 5<sup>th</sup> Biot Conference on Poromechanics)
- Increase in permeability by 18.8% (drag forces?).

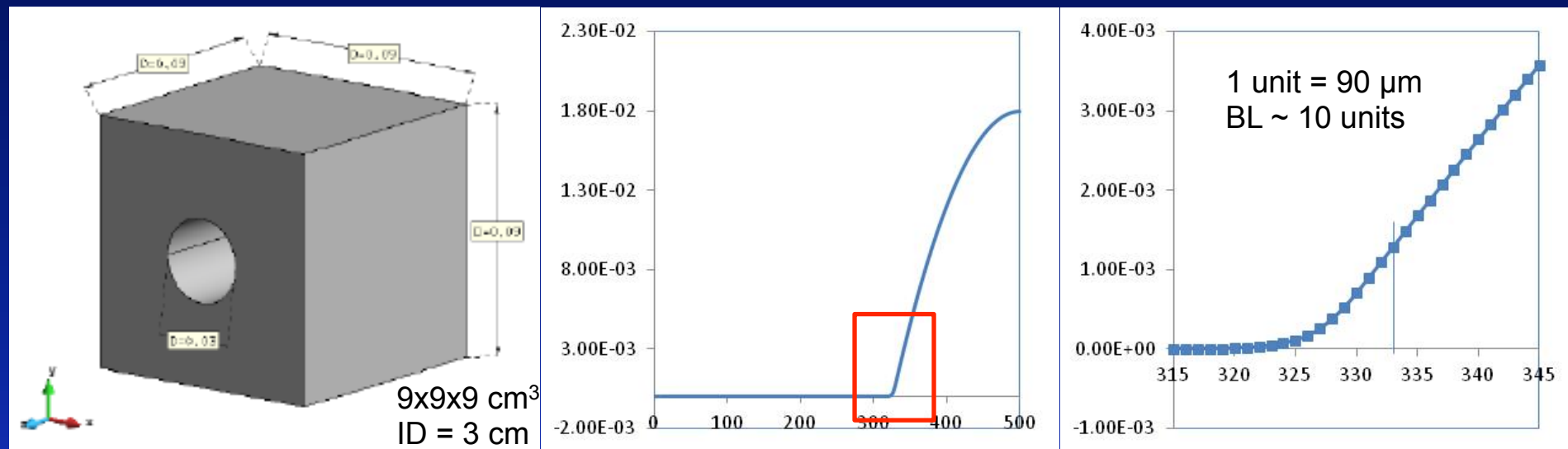


Figure 6: Modeling with LBM





# Approach

- Numerical modeling of a 2D grid consisting of 1) low permeability region and 2) high permeability region:
  - Use FD and Darcy law.
  - Scenario 1:  $k_{mx} \neq 0$  (under investigation)
  - Scenario 2:  $k_{mx} = 0$  (current approach)
  - Compare normal and tangential velocity components  $\rightarrow$  investigate flux.



# Modeling

- Constructing the model:
  - Region 1 & 2.
  - Initial pressure.
  - Closed boundary (no flow) —
  - Permeable interface - -
  - Producing well in high permeability region.

Table 1: Input Data Used for Initial Runs

Region 1	Region 2
Permeability = 1 $\mu$ D	Permeability = 100 mD
Porosity = 5%	Porosity = 35%
Fluid viscosity = 0.5 cP	
Initial Pressure = 7,000 psi	
Producing BHP = 3,000 psi	

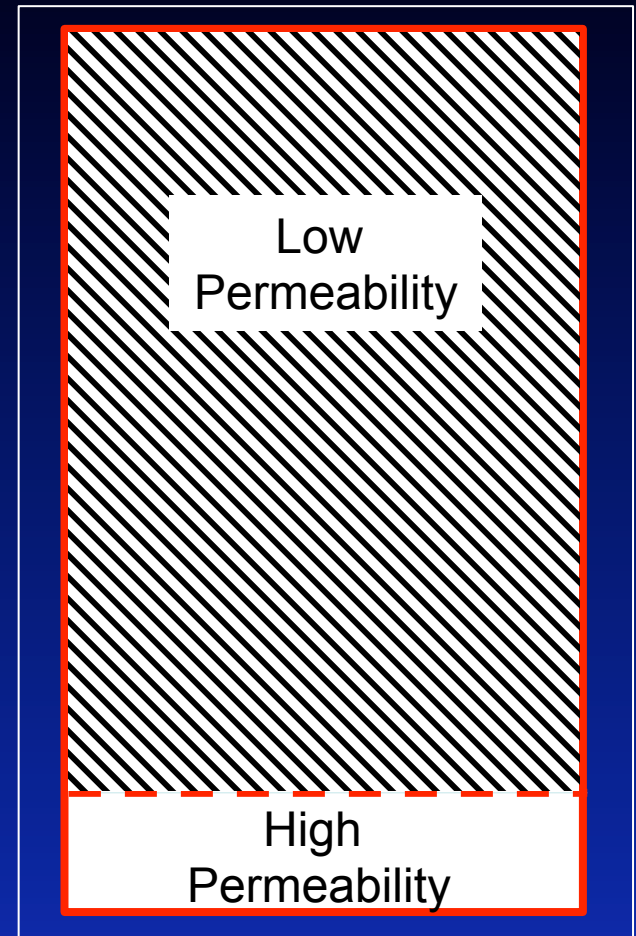


Figure 7: Constructing the Problem



# Modeling & Results: 1<sup>st</sup> Stage

- Modeling I:  
Results Indicated  
that for current  
approach ( $k_{mx} = 0$ )  
mass flux is greater,  
but by **insignificant  
amount (<1%)**.

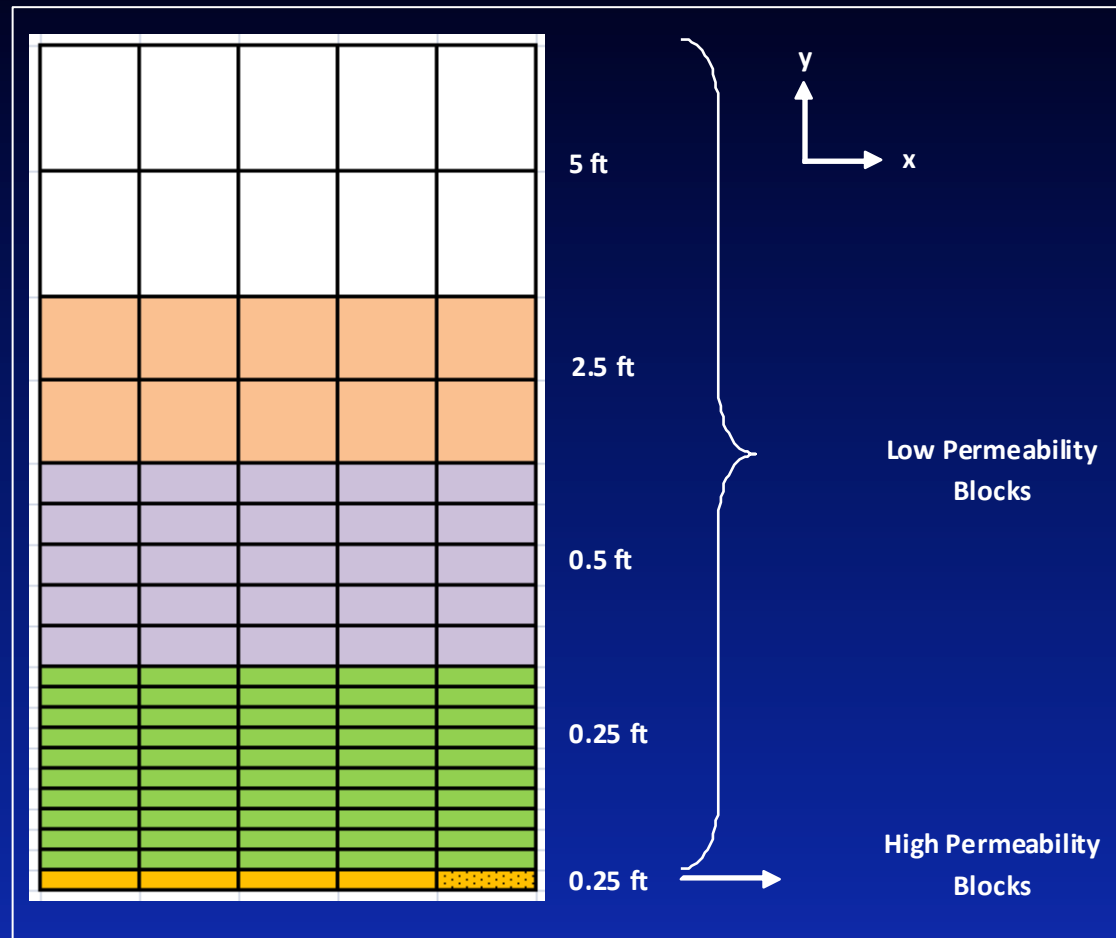


Figure 8: of Initial Modeling Grid



# Modeling & Results: 2<sup>nd</sup> Stage

- Modeling II:
- More refined grid.
- Same conclusion as 1<sup>st</sup> Stage; scenario 2 ( $k_{mx} = 0$ ) mass flux is greater, but by **insignificant amount (<1%)**.
- Based on these conclusions, our decision could be **STOP**.

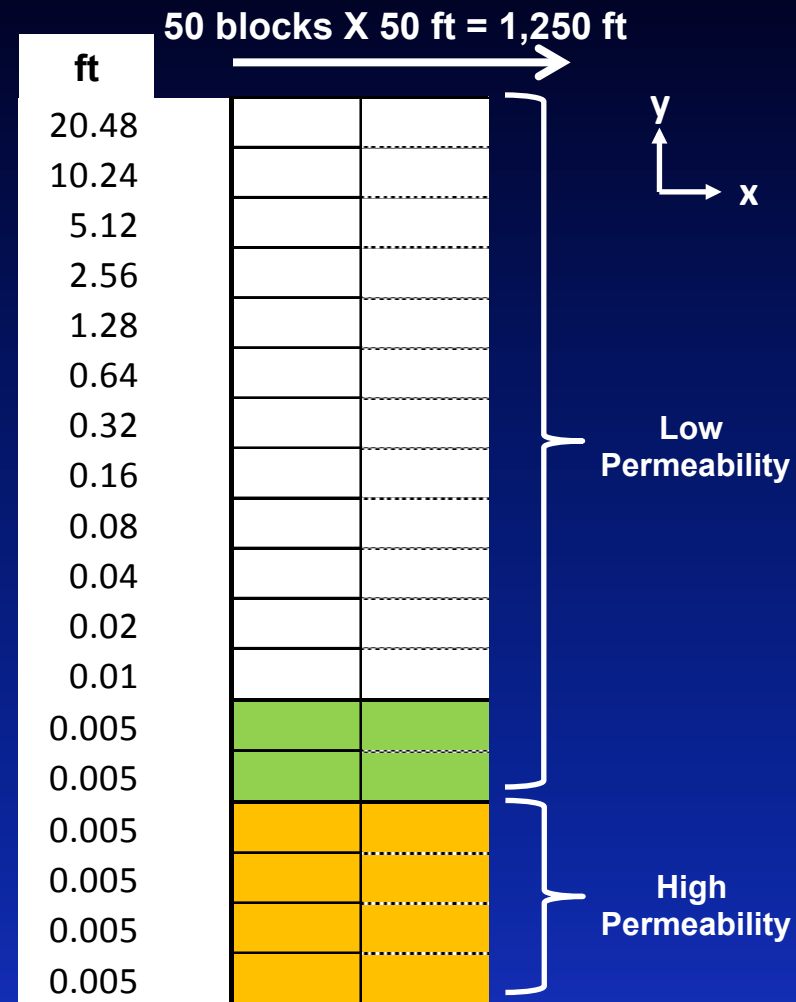


Figure 9: Refined Grid 2<sup>nd</sup> Stage



# Modeling & Results: 2<sup>nd</sup> Stage

- The investigated transition zone is very thin (small scale).
- Do we need different set of tools (math), scale or geometry to study the problem?
- We are not satisfied with previous conclusions; velocity contribution to flux can be calculated.



# Modeling & Results: 3<sup>rd</sup> Stage

- COMSOL 4.3a: Multi-physics platform using Fluid Flow in Porous Media Module.
- Constructing the model:
- Need to look at a smaller scale  
→ Model size: 1"X1"
- Apply similar flow/boundary conditions and input data.

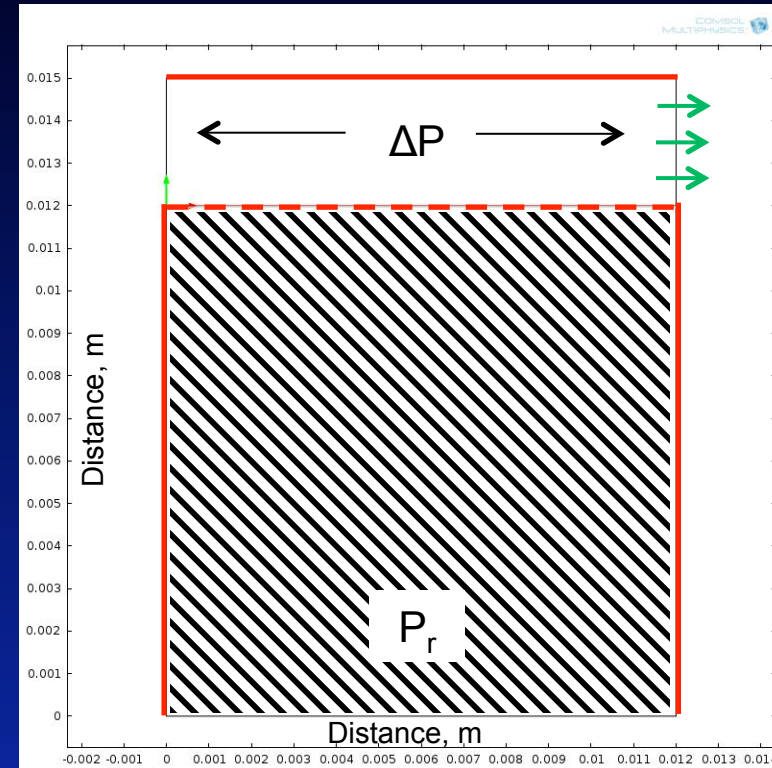


Figure 10: COMSOL Grid

Closed boundary (no flow) —

Permeable interface - -



# Modeling & Results: 3<sup>rd</sup> Stage

- Generate a very dense/fine mesh.
- Results are similar to former modeling cases.

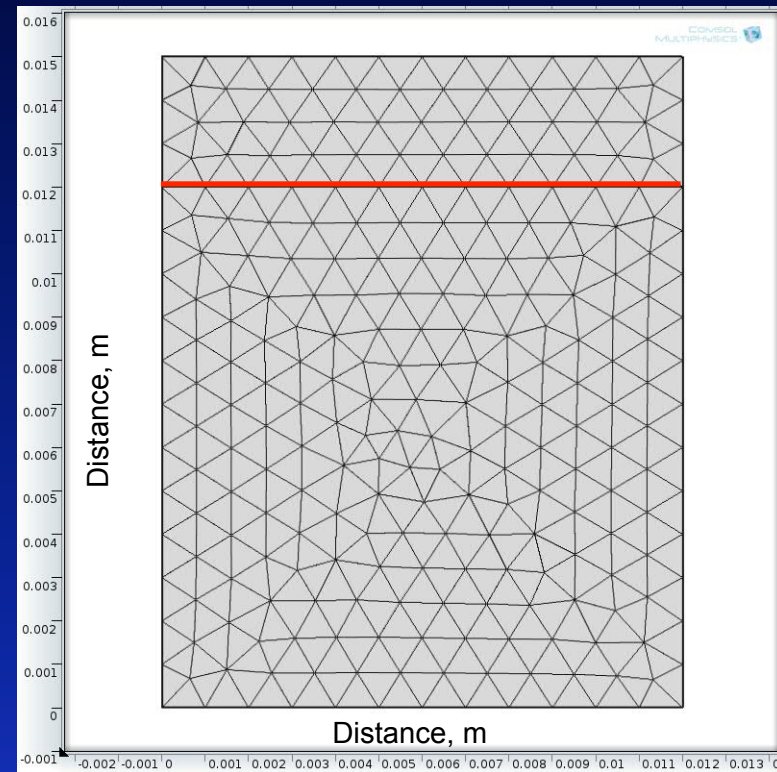


Figure 11: Example of Normal Mesh



# Modeling & Results

- Are we doing something wrong?
- Validation run using the same properties (k and  $\phi$ ), ~~low and high conductivity regions~~; one single domain.
- Is our suggestion ( $k_{mx} \neq 0$ ) and expectations (drag forces) valid?





# Modeling & Results

- Results support our suggestion; **average difference of 11.75%.**

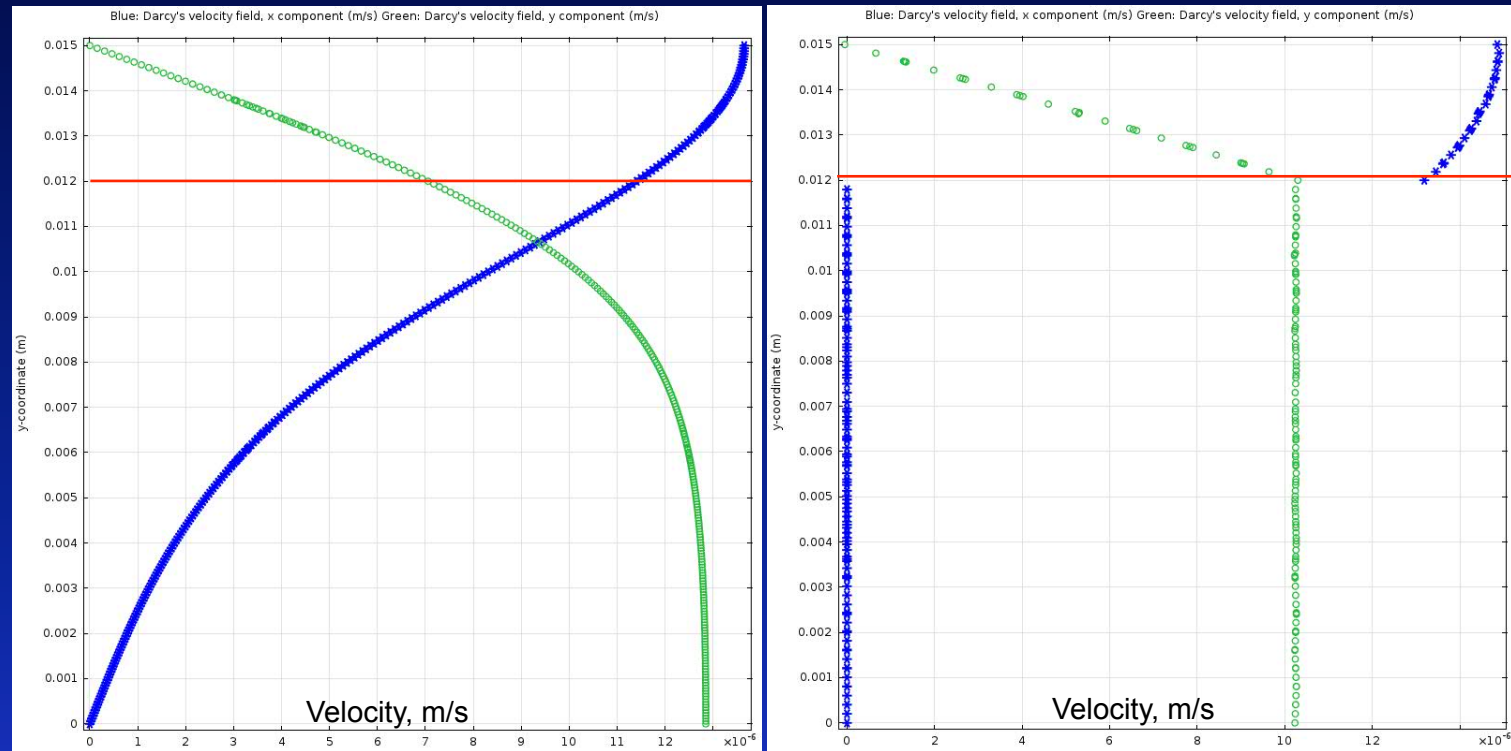


Figure 12: Validation Run Velocity Components



# Modeling & Results

- Boundary conditions can influence the flow behavior.

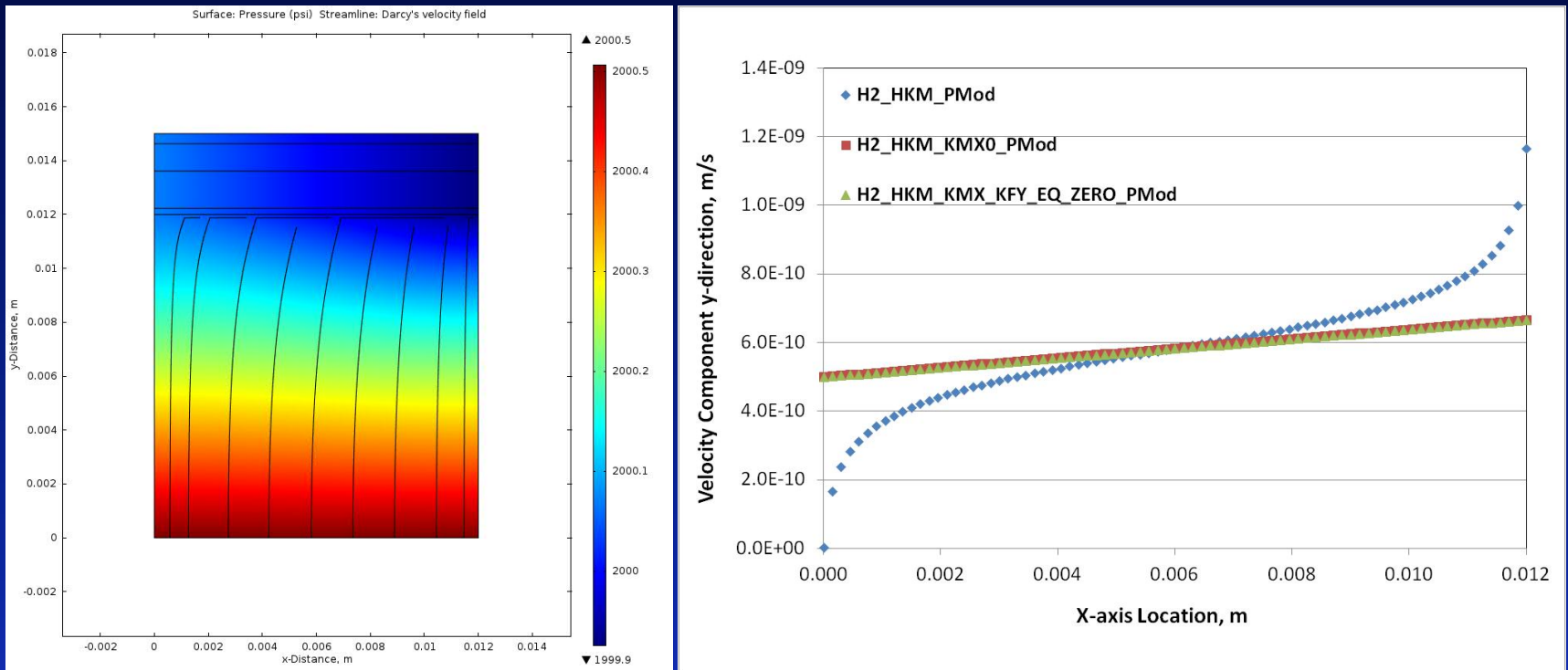


Figure 13: Pressure and Velocity Plots; Various Setup



# What's Next?

- We **might** have possible contribution from tangential velocity.
- Continue investigation:
  - Contrast of properties ( $k$  and  $\phi$ ) is one issue.
  - Try to justify different results and build appropriate model (boundary)
  - Is it possible to generalize the results in the form of a conventional transfer function?
  - How can we incorporate the results into large-scale flow models



# Acknowledgement

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# Thank you

